California Environmental Protection Agency
AIR RESOURCES BOARD

CALIFORNIA NON-METHANE ORGANIC GAS
TEST PROCEDURES

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Monitoring and Laboratory Division, Southern Laboratory Branch
Mobile Source Division
9528 Telstar Avenue
El Monte, California 91731

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APPENDICES

Part A

GENERAL APPLICABILITY AND REQUIREMENTS

1.   These test procedures shall apply to all 1993 and subsequent model-year transitional low-emission vehicles (TLEV), low-emission vehicles (LEV), ultra-low-emission vehicles (ULEV), and super-ultra-low-emission vehicles (SULEV) certifying to non-methane organic gas (NMOG) emission standards.

2.   This document sets forth the analysis and calculation procedures that shall be performed to determine NMOG mass emissions. The document consists of the following parts:

   A.   General Applicability and Requirements
   B.   Determination of Non-Methane Hydrocarbon Mass Emissions by Flame Ionization Detection
   C.   Determination of Alcohols in Automotive Source Samples by Gas Chromatography (Method No. 1001)
   D.   Determination of C_2 to C_5 Hydrocarbons in Automotive Source Samples by Gas Chromatography (Method No. 1002)
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   G.   Determination of NMOG Mass Emissions

Appendix 1   List of Light-End and Mid-Range Hydrocarbons
Appendix 2   Definitions and Commonly Used Abbreviations
Appendix 3   References

Alternative procedures may be used if shown to yield equivalent results and if approved in advance by the Executive Officer of the Air Resources Board.

3.   The analyses specified in the table below shall be performed to determine mass emission rates of NMOG in grams per mile (g/mi) or milligrams per mile (mg/mi) for vehicles operated on the listed fuel:

Fuel	NMHC by FID	NMHC by GC	Alcohols	Carbonyls
Alcohol	X		X	X
CNG		X		X
Diesel	X			X
Gasoline	X			X
LPG	X			X

As Amended: March 22, 2012
Board Hearing: January 26-27, 2012

The specified analyses shall be performed in accordance with the following parts of this document:

NMHC by FID--	Part B.	Determination of Non-Methane Hydrocarbon Mass Emissions by Flame Ionization Detection
NMHC by GC--	Part D.	Determination of C_2 to C_5 Hydrocarbons in Automotive Source Samples by Gas Chromatography (Method No. 1002); and
	Part E.	Determination of C_6 to C_{12} Hydrocarbons in Automotive Source Samples by Gas Chromatography (Method No. 1003)
CARBONYLS--	Part F.	Determination of Aldehyde and Ketone Compounds in Automotive Source Samples by High Performance Liquid Chromatography (Method No. 1004)
ALCOHOLS --	Part C.	Determination of Alcohols in Automotive Source Samples by Gas Chromatography (Method No. 1001)

4. For those manufacturers that choose to develop reactivity adjustment factors unique to a specific engine family, exhaust NMOG emissions shall be fully speciated. NMHC emissions shall be analyzed in accordance with parts D and E (Method Nos. 1002 and 1003). In addition, aldehydes and ketones, alcohols, and ethers shall be analyzed according to parts F, C, and E (Method Nos. 1004, 1001, and 1003). Analysis for alcohols shall be required only for vehicles that are operated on fuels containing alcohols.

5. For natural gas-fueled vehicles, the methane concentration in the exhaust sample shall be measured with a methane analyzer. A GC combined with a FID is used for direct measurement of methane concentrations. SAE Recommended Practice J1151 is a reference on generally accepted GC principles and analytical techniques for this application. A density of 18.89 g/ft^3 shall be used to determine the methane mass emissions. The methane mass emissions shall be multiplied by the appropriate methane reactivity adjustment factor and then added to the reactivity-adjusted NMOG emissions as specified in the "California Exhaust Emission Standards and Test Procedures for 1988-2000 Model Passenger Cars, Light-Duty Trucks, and Medium-Duty Vehicles" and in the "California Exhaust Emission Standards and Test Procedures for 2001 and Subsequent Model Passenger Cars, Light-Duty Trucks, and Medium-Duty Vehicles."

6. The mass of NMOG emissions shall be calculated in accordance with part G, "Determination of NMOG Mass Emissions". The mass of NMOG emissions in g/mile or mg/mile shall be calculated by summing the mass of NMHC determined by the FID, the mass of aldehydes and ketones, and the mass of alcohols.

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PART B

**DETERMINATION OF NON-METHANE HYDROCARBON MASS EMISSIONS
BY FLAME IONIZATION DETECTION**

1.   INTRODUCTION

1.1   This procedure describes a method for determining NMHC exhaust mass emissions from motor vehicles. Other applicable forms of instrumentation and analytical techniques which prove to yield equivalent results to those specified in this procedure may be used subject to the approval of the Executive Officer of the Air Resources Board.

1.2   All definitions and abbreviations are contained in Appendix 2 of these test procedures.

2.   TOTAL HYDROCARBON MEASUREMENT

2.1   A FID is used to measure total hydrocarbon concentration in vehicle exhaust in accordance with the Code of Federal Regulations [Ref.1]. SAE Recommended Practices J254 [Ref. 2] and J1094a [Ref. 3] are references on generally accepted gas analysis and constant volume sampling techniques. For Beckman 400 FIDs only, implementation of the recommendations outlined in SAE paper 770141[Ref. 4] shall be required. Other FID analyzer models shall be checked and adjusted, if necessary, to minimize any non-uniformity of relative response to different hydrocarbons.

3.   METHANE MEASUREMENT

3.1   A GC combined with a FID constitute a methane analyzer and shall be used for direct measurement of methane concentrations. The SAE Recommended Practice J1151[Ref. 5] is a reference on generally accepted GC principles and analytical techniques for this specific application.

4.   TOTAL HC FID RESPONSE TO METHANE

4.1   The FID is calibrated to propane and therefore tends to over respond to the methane portion of the vehicle exhaust sample during hydrocarbon analysis. In order to calculate the NMHC concentration, a methane response factor must be applied to the methane concentration (as measured by the methane analyzer) before it can be deducted from the total hydrocarbon concentration. To determine the total hydrocarbon FID response to methane, known methane in air concentrations traceable to NIST shall be analyzed by the FID. Several methane concentrations shall be analyzed by the FID in the range of the exhaust sample concentration. The total hydrocarbon FID response to methane is calculated as follows:

$$r_{CH_4} = FID_{ppm}/SAM_{ppm}$$

where:

r_{CH_4} = FID methane response factor.
FID_{ppm} = FID reading in ppmC.
SAM_{ppm} = the known methane concentration in ppmC.

The FID response to methane shall be checked at each calibration interval.

5. NMHC MASS EMISSION PER TEST PHASE

5.1   The following calculations shall be used to determine the NMHC mass emissions for each phase of the Federal Test Procedure. [Ref. 1].

5.2   ~~Non-Alcohol Fueled~~ **All** Vehicles

5.2.1 $NMHC_e = FID\ THC_e - (r_{CH_4} * CH_{4e})$
NOTE: If $NMHC_e$ is calculated to be less than zero, then $NMHC_e = 0$.

5.2.2 $NMHC_d = FID\ THC_d - (r_{CH_4} * CH_{4d})$
NOTE: If $NMHC_d$ is calculated to be less than zero, then $NMHC_d = 0$.

5.2.3 $CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$
NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.

a)   For gasoline, $CH_{1.85}$, where HCR = 1.85:
$CO_e = (1 - 0.01925 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

b)   For Phase 2 gasoline, $CH_{1.94}$, where HCR = 1.94:
$CO_e = (1 - 0.01970 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

c)   For LPG, $CH_{2.64}$, where HCR = 2.64:
$CO_e = (1 - 0.02320 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

d)   For CNG, $CH_{3.78}$, where HCR = 3.78:
$CO_e = (1 - 0.02890 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

5.2.4 $$DF = \frac{100 * \left(\dfrac{x}{x + y/2 + 3.76 * (x + y/4 - z/2)} \right)}{CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}}$$

(where fuel composition is $C_xH_yO_z$ as measured for the fuel used.; this expression is generally normalized so that x = 1)

a)   For gasoline, $CH_{1.85}$, where x = 1, y = 1.85, and z = 0:
$DF = 13.47 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}]$

b)   For Phase 2 gasoline, $CH_{1.94}$, x = 1, y = 1.94 and z = 0.017:
       DF = 13.29 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]

       c)   For LPG, $CH_{2.64}$, where x = 1, y = 2.64, and z = 0:
              DF = 11.68 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]

d)   For CNG, $CH_{3.78}$, where x = 1, y = 3.78, and z = 0.016:
              DF = 9.83 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]

e)   For E85, $CH_{2.7841}O_{0.3835}$, Where x = 1, y = 2.7841, and z = 0.3835:
              DF = 12.4253 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]

5.2.5   The density of the NMHC is determined using the carbon:hydrogen ratio of the fuel,
        $C_xH_yO_z$, according to the following equation:

$$NMHC_{dens} = (x * 12.01115 + y * 1.00797)(g/mole) * \left(\frac{28.316847\ liter/ft3}{24.055\ liter/mole} \right)$$

where: 12.01115 = atomic weight of carbon
       1.00797   = atomic weight of hydrogen

5.3   Vehicles Operating on Fuels Containing Methanol

5.3.1 $NMHC_e$ = FID THC_e − (r_{CH_4} * CH_{4e}) − (r_{CH_3OH} * CH_3OH_e)
        NOTE: If $NMHC_e$ is calculated to be less than zero, then $NMHC_e$ = 0.

5.3.2 $NMHC_d$ = FID THC_d − (r_{CH_4} * CH_{4d}) − (r_{CH_3OH} * CH_3OH_d)
        NOTE: If $NMHC_d$ is calculated to be less than zero, then $NMHC_d$ = 0.

5.3.3 CO_e = (1 − (0.01 + 0.005 * HCR) * CO_{2e} − 0.000323 * R_a) * CO_{em}
        NOTE: If a CO instrument which meets the criteria specified in CFR 40 86.111 is used
        and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.

        a)   For M100 (100% methanol), CH_3OH, where HCR = 4:
               CO_e = (1 − 0.03000 * CO_{2e} − 0.000323 * R_a) * CO_{em}

        b)   For M85 (85% methanol, 15% indolene), $CH_{3.41}O_{0.72}$, where
              HCR = 3.41:
               CO_e = (1 − 0.02705 * CO_{2e} − 0.000323 * R_a) * CO_{em}

5.3.4 $$DF = \frac{100 * \left(\dfrac{x}{x + y/2 + 3.76 * (x + y/4 - z/2)} \right)}{CO_{2e} + \left(NMHC_e + CH_{4e} + CO_e + CH_3OH_e + HCHO_e \right) * 10^{-4}}$$

        (where fuel composition is $C_xH_yO_z$ as measured for the fuel used.)

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a) For M100 (100% methanol), CH_3OH, where x = 1, y = 4, and z = 1:
$DF = 11.57 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + CH_3OH_e + HCHO_e) * 10^{-4}]$
b) For M85 (85% methanol, 15% Indolene), $CH_{3.41}O_{0.72}$, where x = 1, y = 3.41, and z = 0.72:
$DF = 12.02 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + CH_3OH_e + HCHO_e) * 10^{-4}]$

5.4 Vehicles Operating on Fuels Containing Ethanol

5.4.1 $NMHC_e = FID\ THC_e - (r_{CH_4} * CH_{4e}) - (r_{C_2H_5OH} * C_2H_5OH_e)$
NOTE: If $NMHC_e$ is calculated to be less than zero, then $NMHC_e = 0$

5.4.2 $NMHC_d = FID\ THC_d - (r_{CH_4} * CH_{4d}) - (r_{C_2H_5OH} * C_2H_5OH_d)$
NOTE: If $NMHC_d$ is calculated to be less than zero, then $NMHC_d = 0$

5.4.3 $CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$
NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.
a) For E100 (100% ethanol), C_2H_5OH, where HCR = 3:
$CO_e = (1 - 0.02500 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

5.4.4 $$DF = \frac{100 * \left(\frac{x}{x + y/2 + 3.76 * (x + y/4 - z/2)} \right)}{CO_{2e} + (NMHC_e + CH_{4e} + CO_e + C_2H_5OH_e + HCHO_e) * 10^{-4}}$$

(where fuel composition is $C_xH_yO_z$ as measured for the fuel used.)

a) For E100 (100% ethanol), C_2H_5OH, where x = 1, y = 3, and z = 0.5:
$DF = 12.29 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + C_2H_5OH_e + HCHO_e) * 10^{-4}]$

5.5 All Vehicles

5.2.6 $NMHC_{conc} = NMHC_e - NMHC_d * [1 - (1 / DF)]$
NOTE: If $NMHC_{conc}$ is calculated to be less than zero, then $NMHC_{conc} = 0$

5.2.7 $NMHC_{mass_n} = NMHC_{conc} * NMHC_{dens} * VMIX * 10^{-6}$

6. TOTAL WEIGHTED NMHC MASS EMISSIONS

6.1 All Vehicles

6.1.1 $NMHC_{wm} = 0.43 * \left(\frac{NMHC_{mass1} + NMHC_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{NMHC_{mass3} + NMHC_{mass2}}{D_{phase3} + D_{phase2}} \right)$

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7. SAMPLE CALCULATIONS

7.1 Given the following data for a gasoline vehicle operated on phase 2 certification fuel, $CH_{1.964}O_{0.0182}$, calculate the weighted NMHC mass emission.

Test Phase	FID THC$_e$ (ppmC)	FID THC$_d$ (ppmC)	CH$_{4e}$ (ppmC)	CH$_{4d}$ (ppmC)	CO$_{em}$ (ppm)	CO$_{2e}$ (%)	VMIX (ft^3)	D$_{phase\ n}$ (mile)	R$_a$ (%)
1	21.928 ~~141.8~~	3.557 ~~8.6~~	3.667 ~~7.53~~	2.545 ~~5.27~~	94.758 ~~147.2~~	0.9581 ~~1.19~~	2745 ~~2846~~	3.610 ~~3.583~~	~~38~~
2	3.826 ~~13.0~~	3.533 ~~8.4~~	2.694 ~~5.68~~	2.490 ~~5.10~~	16.516 ~~20.8~~	0.5925 ~~0.80~~	4700 ~~4856~~	3.876 ~~3.848~~	~~38~~
3	4.242 ~~15.4~~	3.386 ~~8.9~~	2.769 ~~6.16~~	2.414 ~~5.20~~	11.524 ~~36.7~~	0.8225 ~~1.04~~	2738 ~~2839~~	3.611 ~~3.586~~	~~38~~

For Phase 1:

$NMHC_e$ = FID THC$_e$ - (r_{CH_4} * CH$_{4e}$)

= 21.928 ~~41.8~~ ppmC - (1.15 ~~1.04~~ * 3.667 ~~7.53~~ ppmC)

= 17.711 ~~33.97~~ ppmC

$NMHC_d$ = FID THC$_d$ - (r_{CH_4} * CH$_{4d}$)

= 3.557 ~~8.6~~ ppmC - (1.15 ~~1.04~~ * 2.545 ~~5.27~~ ppmC)

= 0.630 ~~3.12~~ ppmC

~~CO$_e$ = (1 - 0.01925 * CO$_{2e}$ - 0.000323 * R$_a$) * CO$_{em}$~~
~~NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO$_{em}$ must be substituted directly for CO$_e$.~~

~~= (1 - 0.01925 * 1.19% - 0.000323 * 38%) * 147.18 ppm~~
~~= 142.0 ppm~~

The numerator of the DF

= 100 * (x / (x + y/2 + 3.76 * (x + y/4 – z/2))

= 100 * (1 / 1 + 1.964 / 2 + 3.76 * (1 + 1.964 / 4 – 0.0182 / 2)

= 13.2381

DF = 13.2381 ~~13.47~~ $\div$ [CO$_{2e}$ + (NMHC$_e$ + CH$_{4e}$ + CO$_e$) * 10^{-4}]

$$DF = \frac{13.2381}{0.9581 + (17.711\ ppmC + 3.667\ ppmC + 94.758\ ppmC) * 10^{-4}}$$

$$\text{~~DF = }\frac{\text{13.47}}{\text{1.19\% + (33.97 ppmC + 7.53 ppmC + 142.0 ppmC) * 10}^{-4}}$$

= ~~11.15~~ 13.653

$NMHC_{conc}$ = NMHC$_e$ - NMHC$_d$ * [1 - (1 $\div$ DF)]
= ~~33.97 ppmC - 3.12 ppmC * [1 - (1 ÷ 11.15)]~~

$$= 17.711 \text{ ppmC} - 0.630 \text{ ppmC} * [1 - (1 \div 13.653)]$$
$$= \underline{17.127} \; \cancel{31.13} \; \text{ppmC}$$

$$NMHC_{dens} = (x * 12.01115 + y * 1.00797)(g / mole) * \left(\frac{28.316847 \text{liter/ft3}}{24.0547 \text{liter/mole}} \right)$$

$$\underline{NMHC_{dens}} = (1 * 12.01115 + 1.964 * 1.00797) * (28.316847/24.055)$$
$$= 16.470 \text{ g/ft}^3$$

$$NMHC_{\text{mass n}} = NMHC_{conc} * NMHC_{dens} * VMIX * 10^{-6}$$
$$= \underline{17.127} \; \cancel{31.13} \text{ ppmC} * 16.\underline{47}\cancel{33} \text{ g/ft}^3 * \underline{2745} \; \cancel{2846} \text{ ft}^3 * 10^{-6}$$

$$NMHC_{\text{mass 1}} = \underline{0.7743} \; \cancel{1.45} \text{ g}$$

Similarly, for Phase 2: $NMHC_{\text{mass 2}} = \underline{0.0068} \; \cancel{0.33} \text{ g}$
and for Phase 3: $NMHC_{\text{mass 3}} = \underline{0.0219} \; \cancel{0.27} \text{ g}$

Therefore,

$$NMHC_{wm} = 0.43 * \left(\frac{NMHC_{mass1} + NMHC_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{NMHC_{mass3} + NMHC_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$\cancel{NMHC_{wm} = 0.43 * \left(\frac{1.45 \text{ g} + 0.33 \text{ g}}{3.583 \text{ miles} + 3.848 \text{ miles}} \right) + 0.57 * \left(\frac{0.27 \text{ g} + 0.33 \text{ g}}{3.586 \text{ miles} + 3.848 \text{ miles}} \right)}$$

$$NMHC_{wm} = 0.43 * \left(\frac{0.768 \text{ g} + 0.0068 \text{ g}}{3.610 \text{ miles} + 3.876 \text{ miles}} \right) + 0.57 * \left(\frac{0.0217 \text{ g} + 0.0068 \text{ g}}{3.611 \text{ miles} + 3.876 \text{ miles}} \right)$$

$$NMHC_{wm} = \underline{0.047} \; \cancel{0.15} \text{ g/mile}$$

7.2 Given the following data for a vehicle operating on $\underline{10}\cancel{85}$% ~~m~~ethanol and $\underline{90}\cancel{15}$% gasoline ($\underline{E10}$ ~~M-85~~) $CH_{2.7841}O_{0.3835}$, calculate the weighted NMHC mass emission.

~~Test Phase~~	~~FID THC$_e$ (ppmC)~~	~~FID THC$_d$ (ppmC)~~	~~CH$_{4e}$ (ppmC)~~	~~CH$_{4d}$ (ppmc)~~	~~CH$_3$OH$_e$ (ppm)~~	~~CO$_{em}$ (ppm)~~	~~CO$_{2e}$ (%)~~	~~VMIX (ft^3)~~	~~D$_{phase\,n}$ (mile)~~	~~R$_a$ (%)~~	~~HCHO$_e$ (ppm)~~
~~1~~	~~88.5~~	~~5.5~~	~~17.76~~	~~2.82~~	~~72.9~~	~~303.2~~	~~1.28~~	~~2832~~	~~3.570~~	~~32~~	~~0.96~~
~~2~~	~~14.5~~	~~7.0~~	~~8.01~~	~~2.82~~	~~5.1~~	~~9.7~~	~~0.83~~	~~4827~~	~~3.850~~	~~32~~	~~0.10~~
~~3~~	~~21.8~~	~~7.7~~	~~10.13~~	~~2.93~~	~~7.4~~	~~18.2~~	~~1.13~~	~~2825~~	~~3.586~~	~~32~~	~~0.12~~

Test Phase	FID THC$_e$ (ppmC)	FID THC$_d$ (ppmC)	CH$_{4e}$ (ppmC)	CH$_{4d}$ (ppmC)	CO$_{em}$ (ppm)	CO$_{2e}$ (%)	VMIX (ft^3)	D$_{phase\ n}$ (mile)
1	14.398	2.971	3.639	2.125	97.83	0.9203	3508	3.590
2	2.882	2.830	2.176	2.010	12.25	0.5935	6010	3.858
3	3.976	2.642	2.621	2.058	19.86	0.7624	3502	3.581

[For this example, CH₃OH$_d$ was assumed to be 0.0 ppmC for all three background bag samples.]

For Phase 1:

NMHC$_e$ = FID THC$_e$ - (r_{CH_4} * CH$_{4e}$) ~~- (r_{CH_3OH} * CH₃OH$_e$)~~

= 14.398 ~~88.5~~ ppmC - (1.15 ~~1.04~~ * 2.215 ~~17.76~~ ppmC) ~~- (0.66*72.9 ppmC)~~

= 10.213 ~~21.92~~ ppmC

NMHC$_d$ = FID THC$_d$ - (r_{CH_4} * CH$_{4d}$) ~~- (r_{CH_3OH} * CH₃OH$_d$)~~

= 2.971 ~~5.5~~ ppmC - (1.15 ~~1.04~~ * 2.125 ~~2.82~~ ppmC) ~~- (0.66*0.0 ppmC)~~

= 0.527 ~~2.57~~ ppmC

~~CO$_e$ = (1 - 0.02705 * CO$_{2e}$ - 0.000323 * R$_a$) * CO$_{em}$~~
~~NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO$_{em}$ must be substituted directly for CO$_e$.~~

~~= (1 - 0.02705 * 1.28% - 0.000323 * 32%) * 303.2 ppm~~
~~= 289.6 ppm~~

DF = 13.511 ~~12.02~~ ÷ [CO$_{2e}$ + (NMHC$_e$ + CH$_{4e}$ + CO$_e$ ~~+ CH₃OH$_e$ + HCHO$_e$~~) * 10^{-4}]

$$= \frac{12.02}{1.28\% + \left(21.92\,ppmC + 17.76\,ppmC + 289.6\,ppmC + 72.9\,ppmC + 0.96\,ppmC\right)*10^{-4}}$$

$$= \frac{13.511}{0.9203 + \left(10.213\,ppmC + 3.639\,ppmC + 97.83\,ppmC\right)*10^{-4}}$$

= 14.505 ~~9.10~~

NMHC$_{conc}$ = NMHC$_e$ - NMHC$_d$ * [1 - (1 / DF)]

= 10.213 ~~21.92~~ ppmC – 0.527 ~~2.57~~ ppmC * [1 - (1 / 14.505 ~~9.10~~)]

= 9.722 ~~19.63~~ ppmC

NMHC$_{mass\ n}$ = NMHC$_{conc}$ * NMHC$_{dens}$ * VMIX * 10^{-6}

NMHC$_{mass\ 1}$ = 0.558 ~~0.91~~ g

Similarly, Phase 2: $\text{NMHC}_{\text{mass 2}} = 0.0\ \text{g}$
and for Phase 3: $\text{NMHC}_{\text{mass 3}} = \text{0.10}\ \underline{0.040}\ \text{g}$

Therefore,

$$\text{NMHC}_{\text{wm}} = 0.43 * \left(\frac{\text{NMHC}_{\text{mass1}} + \text{NMHC}_{\text{mass2}}}{\text{D}_{\text{phase1}} + \text{D}_{\text{phase2}}} \right) + 0.57 * \left(\frac{\text{NMHC}_{\text{mass3}} + \text{NMHC}_{\text{mass2}}}{\text{D}_{\text{phase3}} + \text{D}_{\text{phase2}}} \right)$$

$$\text{NMHC}_{\text{wm}} = 0.43 * \left(\frac{0.91\,\text{g} + 0.00\,\text{g}}{3.570\ \text{miles} + 3.850\ \text{miles}} \right) + 0.57 * \left(\frac{0.10\,\text{g} + 0.00\,\text{g}}{3.586\ \text{miles} + 3.850\ \text{miles}} \right)$$

$$\text{NMHC}_{\text{wm}} = 0.43 * \left(\frac{0.558\,\text{g} + 0.00\,\text{g}}{3.590\ \text{miles} + 3.858\ \text{miles}} \right) + 0.57 * \left(\frac{0.040\,\text{g} + 0.00\,\text{g}}{3.581\ \text{miles} + 3.858\ \text{miles}} \right)$$

$\text{NMHC}_{\text{wm}} \quad = \text{0.06 g/mile}$

$\underline{\text{NMHC}_{\text{wm}} \quad = 0.035\ \text{g/mile}}$

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Part C

**DETERMINATION OF ALCOHOLS
IN AUTOMOTIVE SOURCE SAMPLES
BY GAS CHROMATOGRAPHY**

METHOD NO. 1001

1. **INTRODUCTION**

1.1 This document describes a method of sampling and analyzing automotive source samples ~~exhaust~~ for alcohols ~~in the range of 1 to 1200 µg per 15 mL of solution. The "target" alcohols that shall be analyzed and reported by this method are methanol and ethanol. These alcohols, when measured in concentrations above the LOD, shall be reported~~.

1.2 This procedure is based on a method developed by the U. S. Environmental Protection Agency, (U.S. EPA) [Ref -6] which involves flowing diluted engine exhaust through deionized or purified water contained in glass impingers and analyzing this solution by gas chromatography~~-~~.

1.3 The "target" alcohols (compounds of interest) that shall be measured by this method are methanol and ethanol in the range of 1 to 1200 µg per 15 mL of impinger solution. These alcohols, when measured in concentrations above the LOD, shall be reported.

    1.3.1 For the purpose of calculating NMOG for vehicles tested on exhaust emission test fuel containing ethanol (see Part G, Determination of NMOG Mass Emissions):

    1.3.1.1 The only alcohol that needs to be reported from this method is ethanol.

    1.3.1.2 The analysis of methanol is also within the scope of this analytical method and its measurement may provide meaningful information to the laboratory. However, its measurement is not required.

1.4 Other applicable forms of instrumentation and analytical techniques may be used if shown to yield results equivalent to those specified in this procedure and if approved in advance by the Executive Officer of the Air Resources Board.

1.5 All definitions and abbreviations are contained in Appendix 2 of these test procedures.

2.   **METHOD SUMMARY**

2.1   The samples are received by the laboratory in impingers. Compound separation and analysis are performed using a GC. The sample is injected into the GC by means of a liquid autosampler. Separation of the sample mixture into its components is performed by a temperature-programmed capillary column. A FID is used for alcohol detection and quantification.

2.2   The computerized GC data system identifies the alcohol associated with each peak. The alcohol concentrations are determined by integrating the peak areas and using response factors determined from external standards.

3.   **INTERFERENCES AND LIMITATIONS**

3.1   An ~~interferent~~ interfering compound is any component present in the sample with a retention time similar to that of any target alcohol described in this method. To reduce interference error, proof of chemical identity may require periodic confirmations using an alternate method and/or instrumentation, e.g., GC/MS.

3.2   The concentration of the alcohols in the range of interest is stable for up to six days as long as the samples are sealed and refrigerated at a temperature below 40°F.

3.3   To avoid sample loss and/or contamination, samples should be analyzed or transferred from the impingers to tightly sealed storage bottles as soon as possible after collection.

4.   **INSTRUMENTATION AND APPARATUS**

4.1   For each mode of the CVS test, two sampling impingers, each containing a known amount of deionized or purified water (e.g. 15 mL for this procedure), are used to contain the sample.

   4.1.1   A temperature-programmable GC, equipped with a DB-Wax type ~~Megabore~~ column ~~(~~[typically 30 m, 0.53 mm ID (Megabore), 1.0 μ film thickness]~~)~~ and FID, is used. Other columns may be used, provided the alternate(s) can be demonstrated to the ARB to be equivalent or better with respect to precision, accuracy and resolution of all the target alcohols.

   4.1.2   A liquid injection autosampler is required.

   4.1.3   A PC-controlled data acquisition system for quantifying peak areas is required.

5. **REAGENTS AND MATERIALS**

5.1   Methanol shall have a purity of 99.9 percent, or be high performance liquid chromatography grade, EM Science or equivalent.

5.2   Ethanol shall be absolute, ACS reagent grade.

5.3   ASTM Type I purified or Type II deionized water shall be used.

5.4   Stock solutions are prepared gravimetrically or volumetrically by diluting methanol and ethanol with deionized or purified water, e.g., for this method a typical stock solution contains approximately 10 mg/mL of each target alcohol. Stock solutions must be replaced at least every six months.

    5.4.1   A **calibration standard** within the expected concentration range of the samples is prepared by successive dilutions of the stock solution with deionized or purified water. ; 3 to 50 µg/mL is typical, depending on fuel type. Calibration standards must be replaced at least every week.

    5.4.1.1 Typical calibration standards range from 3 to 100 µg/mL for exhaust emission testing, depending on fuel type.

    5.4.1.2 Evaporative emission testing may require calibration standards as high as 1000 µg/mL due to higher sample concentration.

    5.4.1.3 Calibration standards must be replaced frequently to avoid degradation of the standard. Standards with concentrations of 100 µg/mL or less should be replaced weekly.

    5.4.2   A **control standard** containing all target alcohols is prepared by successive dilutions of a stock solution different from that of used in Section 5.4.1. This standard, at an approximate concentration of the samples, is used to monitor the precision of the analysis of each target alcohol. Control standards must be replaced at least every week.

    5.4.3   Standards used for linearity and LOD determinations (Section 8) are also prepared by successive dilutions of an appropriate level stock solution.

    5.4.4   Standards may also be purchased (e.g., NIST).

    5.4.5   All standards should be refrigerated at a temperature below 40°F during storage.

5.5   Gas requirements.

    5.5.1   Air shall be "Zero" grade (<1 ppmC total hydrocarbon contamination) or better.

    5.5.2   Nitrogen shall have a minimum purity of 99.998 percent.

    5.5.3   Helium shall have a minimum purity of 99.995 percent.

    5.5.4   Hydrogen shall have a minimum purity of 99.995 percent.

6.   PROCEDURE

6.1   Each of the graduated sampling impingers is filled with 15 mL of deionized or purified water.

6.2   The impingers are placed in an ice bath during the sample collection.

6.3   After sampling, the solution contained in each impinger is transferred to a vial and sealed.

    6.3.1   Samples shall be refrigerated at a temperature below 40°F if immediate analysis is not feasible, or if reanalysis at a later date may be required.

6.4   One microliter aliquots of unmodified samples are injected via autosampler into a GC. ~~Suggested~~ <u>Typical</u> standard operating conditions for the GC are:

Column:	DB-Wax, 30 m, 0.53 mm ID, 1.0µ film thickness
Carrier gas flow:	Helium at 5 mL/min
Make-up gas flow:	Nitrogen at 25 mL/min
Detector:	FID, hydrogen at 30 mL/min and air at 300 mL/min
Injector:	Packed column injector with Megabore adapter insert; on-column injection
Column temperature:	50°C (1 min)~~,~~
	50°C to 70°C (5°C/min)~~,~~
	70°C to 110°C (15°C/min)~~,~~
	110°C (4 min)
Data system:	PC-based data acquisition system

6.5   Samples containing compounds having concentrations above the documented range of instrument linearity must be diluted and reanalyzed.

6.6   The peak integrations are corrected as necessary in the data system. Any misplaced baseline segments are corrected in the reconstructed chromatogram.

6.7   The peak identifications provided by the computer are checked and corrected if necessary.

7.   **CALCULATIONS**

7.1   The concentration of each target alcohol, in µg/mL, is determined by the following calculation that ~~compares~~ relates the sample peak area to ~~with~~ that of an external standard:

Concentration (µg/mL)$_{sample}$ = Peak Area$_{sample}$ x Response Factor

where the response factor (RF) is calculated during the calibration by:

$$RF = \frac{Concentration_{standard\,(\mu g/mL)}}{Peak\;Area_{standard}}$$

7.2   Sample batches that span a broad concentration range (several orders of magnitude) should use more than one calibration level.

7.2.1   Each sample concentration would then be calculated by using a standard of similar concentration to calculate the response factor, as in Section 7.1.

7.2.2   A multipoint calibration curve calculated by the GC software (e.g., Varian Star 6.0) may be used instead of the one-point calibration described in Section 7.1.

7.3   This concentration is then used to calculate the total amount of alcohol in each impinger:

Mass (µg) = Concentration (µg/mL) x Impinger volume (mL)

7.4   An internal standard method may also be used.

8.   **QUALITY CONTROL**

8.1   Blank Run - A deionized or purified water blank is run each analysis day. All target alcohol concentrations from the blank analysis must be below the LOD before the analysis may proceed.

8.1.1   If the blank shows a peak greater than the limit of detection (LOD) in the region of interest, the source of the contamination must be investigated and remedied.

8.2   Calibration Run - The calibration standard is analyzed each analysis day to generate the response factor used to quantify the sample concentrations.

8.3   Control Standard Run - The quality control standard is analyzed at least once each analysis day. Measurements of all target alcohols in the control standard must fall within the control limits to ensure the validity of the sample analyses that day. To meet this requirement, it may be necessary to inspect and repair the GC, and rerun the calibration and/or control standards.

8.4   Control Charts - A quality control chart is maintained for each analyte in the control standard. The control charts, used on a daily basis, establish that the method is "in-control". The following describes how to construct a typical control chart:

1.   Obtain at least 20 daily control standard results;
2.   Calculate the control standard mean concentration and standard deviation for the target analyte; and
3.   Create a control chart for the target analyte by placing the concentration on the Y-axis and the date on the X-axis. Establish upper and lower warning limits at either two standard deviations (2s) or 5 percent, whichever is greater, above and below the average concentration. Establish an upper and lower control limits at either three standard deviations (3s) or 5 percent, whichever is greater, above and below the average concentration.
4.   A control standard measurement is considered to be out-of-control when the analyzed value exceeds the control limit or two successive control standard measurements of the same analyte exceed the warning limit.
5.   If 20 control standard results are not yet available to create a control chart (e.g., the control standard was expended and replaced with a different concentration standard prior to obtaining 20 points with the new standard), measurements must be within 10% of the theoretical concentration.

The measured concentrations of all target analytes contained in the control standard must be within the control limits ("in-control") for the sample results to be considered acceptable.

8.5   Duplicates - A duplicate analysis of one sample is performed at least once per analysis day. The relative percent difference (RPD) is calculated for each duplicate run:

$$\text{RPD}(\%) = \frac{|\text{Difference between duplicate and original measurements}|}{\text{Average of duplicate and original measurements}} * 100$$

For each compound, the allowable RPD depends on the average concentration level for the duplicate runs, as shown in the following table:

Average Measurement for Duplicate Runs		Allowable RPD (%)
1 to 10	times LOD	100
10 to 20	" "	30
20 to 50	" "	20
Greater than 50	" "	15

If the results of the duplicate analyses do not meet these criteria for all target alcohols, the sample may be reanalyzed. If reanalysis is not feasible or if the criteria are still not met on reanalysis, all sample results for that analysis day are invalid.

8.6   Linearity - A multipoint calibration to confirm instrument linearity is performed for all target alcohols for new instruments, after making instrument modifications that can affect linearity, and at least once every year. The multipoint calibration consists of at least five concentration or mass loading levels, each above the LOD, distributed over the range of expected sample concentration. Each concentration level is measured at least twice. A linear regression analysis is performed using concentration and area counts to determine the regression correlation coefficient (r). The r must be greater than 0.995 to be considered sufficiently linear for one point calibrations.

8.7   Limit of Detection - The LOD for the target alcohols must be determined for new instruments, after making instrument modifications that can affect the LOD and at least once every year. To make the calculations, it is necessary to perform a multipoint calibration consisting of at least four "low" concentration levels, each above the expected LOD, with at least five replicate determinations of the lowest concentration standard. A linear regression is performed and the standard deviation (in area counts) of the lowest concentration standard determined. The standard deviation is converted to concentration units using the slope of the linear regression:

$$s = s_a \div m$$

where m is the slope of the linear regression, s is the standard deviation (in concentration units) of the lowest concentration standard and s_a is the standard deviation (in area counts) of the lowest concentration standard.

The LOD must be calculated using the following equation [Ref. 12]:

$$LOD = t * s$$

where s is the standard deviation (in concentration units) of at least five replicate determinations of the lowest concentration standard and t is the t-factor for 99 percent confidence for a one-sided normal (Gaussian) distribution. The number of degrees of freedom is equal to the number of replicates, minus one. An abbreviated t–table is:

Degrees of Freedom	t-value
4	3.7
5	3.4
6	3.1
7	3.0

The lowest standard must be of a concentration of one to five times the estimated LOD.

8.7.1   The maximum allowable LOD for each alcohol is 0.10 µg/mL. The calculated laboratory LOD must be equal to or lower than the maximum allowable LOD. All peaks identified as target compounds that are equal to or exceed the maximum allowable LOD must be reported. If the calculated laboratory LOD is less than the maximum allowable LOD, the laboratory may choose to set its reporting limit at the maximum allowable LOD, the calculated laboratory LOD, or any level in between.

8.7.2   For the purpose of calculating the total mass of all species, the concentrations of the compounds below the LOD are considered to be zero.

Part D

**DETERMINATION OF C$_2$ TO C$_5$ HYDROCARBONS
IN AUTOMOTIVE SOURCE SAMPLES BY GAS CHROMATOGRAPHY**

METHOD NO. 1002

1.   **INTRODUCTION**

1.1   This document describes a gas chromatographic method of ~~analyzing~~ measuring
        C$_2$ to C$_5$ hydrocarbons (light-end hydrocarbons) in the ppbC range from
        automotive source samples. This method does not include sample collection
        procedures [Ref. 8]. The "target" hydrocarbons (compounds of interest) that shall
        be analyzed and reported by this method and Method 1003 are listed in Appendix
        1. All compounds on this list, when measured in concentrations above the LOD,
        shall be measured and reported ("targeted") by either Method 1002 or Method
        1003. Each laboratory should divide the list into light-end (Method 1002) and
        mid-range (Method 1003) hydrocarbons in the manner that best suits the
        laboratory instrumentation. All compounds on the list not targeted by Method
        1002 must be targeted by Method 1003.

1.2   Other applicable forms of instrumentation and analytical techniques may be used
        if shown to yield results equivalent to those specified in this procedure and if
        approved in advance by the Executive Officer of the Air Resources Board.

1.3   All definitions and abbreviations are contained in Appendix 2 of these test
        procedures.

2.   **METHOD SUMMARY**

2.1   This is a method intended for routine analysis.

2.2   The samples are received by the laboratory in ~~Tedlar~~ Kynar® bags, which are
        sub-sampled into a GC for separation and analysis.

2.3   The gas chromatographic analysis is performed on an Alumina (Al$_2$0$_3$) PLOT
        column temperature programmed from 0$^{\text{o}}$C to 200$^{\text{o}}$C. An FID is used for
        detection and quantification.

2.4   The sample is injected into the GC by means of gas sampling valves. Separation
        of the sample hydrocarbon mixture into its components takes place in the
        chromatographic column. The chromatographic column and the corresponding
        operating parameters described in this method normally provide complete
        resolution of most target compounds.

D-1

2.5   The computerized GC data acquisition system identifies the hydrocarbons associated with each peak. The hydrocarbon concentrations are determined by integrating the peak areas and using response factors determined from NIST-traceable standards.

3.   **INTERFERENCES AND LIMITATIONS**

3.1   An ~~interferent~~ interfering compound is any component present in the sample with a retention time very similar to that of any target hydrocarbon described in this method. To reduce interference error, proof of chemical identity may require periodic confirmations using an alternate method and/or instrumentation, e.g., GC/MS, PID, different column, etc.

3.2   To maximize sample integrity, sample bags should not leak or be exposed to bright light or excessive heat. Sampling bags must be shielded from direct sunlight to avoid photochemically induced reactions of any reactive hydrocarbons. The compound 1,3-butadiene, resulting mostly during cold-start testing, is unstable. Therefore all cold-start samples must be analyzed within 8 hours; all other samples must be analyzed within 24 hours, although analysis within 8 hours is recommended.

4.   **INSTRUMENTS AND APPARATUS**

4.1   ~~Tedlar~~ Kynar® (polyvinylidene fluoride) bags, ~~2~~ 4 mil in thickness, nominally 5 to 10 liters in capacity and equipped with quick-connect fittings, are typically used to contain the samples. Other sample collection containers, such as bags made of Tedlar® (polyvinyl fluoride) film or nickel-coated stainless steel canisters, may be used, provided they are made of non-reactive material and do not cause sample loss or contamination.

4.2   For manual sub-sampling into a GC, a ground glass syringe is used to transfer gaseous samples from Tedlar bags to the GC sample inlet. For automated systems, a sample loop is used to transfer gaseous samples from the Tedlar bag to the sample inlet of the GC. Sample aliquot size is chosen based on considerations of instrument sensitivity and/or linearity.

4.3   A temperature-programmable GC equipped with a gas sampling valve system, a FID, and accessories is required.

4.4   An Alumina PLOT column (typically 50 m x 0.32 mm) is used. A wax precolumn is recommended to prevent water damage to the PLOT column. Other columns may be used, provided the alternate(s) can be demonstrated to the ARB to be equivalent or better with respect to precision, accuracy and resolution of all the target hydrocarbons.

4.5   A sample trap capable of being cryogenically cooled may be used.

D-2

4.6   Data acquisition software is used to integrate peak areas to determine hydrocarbon concentrations.

5.   **REAGENTS AND MATERIALS**

5.1   Helium shall have a minimum purity of 99.995 percent. Higher purity helium may be required to achieve the LOD required by Section 8.7.1.

5.2   Hydrogen shall have a minimum purity of 99.995 percent.

5.3   Air shall be "Zero" grade (<1 ppmC total hydrocarbon contamination) or better.

5.4   Nitrogen shall have a minimum purity of 99.998 percent.

5.5   Calibration Standard - The quantitative calibration standard for all target hydrocarbons shall be propane at a concentration level between 0.25 and 1 ppm-mole and within the calculated linearity of the method. (See Section 8.6.) This propane standard must be a NIST-certified SRM or secondary NIST-traceable standard. A secondary standard is obtained by a comparison between a SRM and a candidate standard.

5.6   Control Standard - A quality control standard, containing at least ethene, propane, n-butane, and 2-methylpropene with concentrations between 0.2 and 3 ppmC based on a propane standard, is used for the following purposes:

        1.   Daily update of control charts, and
        2.   Daily determination of marker retention time windows.

5.7   A high concentration standard (higher than the calibration standard), containing the target hydrocarbons listed in Section 5.6, is used for linearity determinations. The high concentration standard must have concentrations verified against a NIST-traceable propane standard. (See Section 5.5 for the definition of NIST-traceable.) This verification can be performed at the laboratory performing the analysis.

5.8   A low concentration standard (one to five times the estimated LOD), containing the target hydrocarbons listed in Section 5.6, is used for LOD determinations. The low concentration standard must have concentrations verified against a NIST-traceable propane standard. (See Section 5.5 for the definition of NIST-traceable.) This verification can be performed at the laboratory performing the analysis.

        5.8.1   In lieu of a low concentration standard, a higher concentration standard may be diluted.

5.9   Liquid nitrogen may be required to cool the cryogenic sample trap and column oven where applicable.

6.   **PROCEDURE**

6.1   The gaseous sample is analyzed for the target hydrocarbons C_2 through C_5.

6.2   ~~Suggested~~ <u>Typical</u> standard operating conditions for the <u>automated gas</u> chromatograph are:

Helium carrier gas <u>flow</u> ~~velocity~~:   ~~30 cm/sec~~ <u>2.2 mL/min at 200^0C</u>
<u>Detector (0.010" FID)</u>
    <u>Temperature:</u>   <u>250^0C or higher</u>
    Nitrogen make-up gas flow: sufficient such that the total flow of helium plus nitrogen is ~~30~~ <u>25</u> mL/min
    Hydrogen gas flow: ~~30~~ <u>25</u> mL/min
    Air flow: 300 mL/min
    <u>Range 12, attenuation 8 (or another suitable value)</u>
Sample <u>loop</u>/valve temperature: 150^0C (PLOT column)
<u>Cryotrap temperature:</u>   <u>-180^0C (hold to trap hydrocarbons)</u>
                                     <u>200^0C (heat to release) hydrocarbons)</u>
<u>Precolumn oven temperature:</u>   <u>50^0C</u>
<u>Analytical column valve oven temperature:</u> <u>150^0C</u>
Column Temperature<u> Program</u>: 0^0C (hold ~~3~~<u>7</u> min)~~,~~
                                    ~~10^0C/min to 200^0C (hold 15 min)~~
                                    <u>5^0C/min to 200^0C</u>
                                    <u>200^0C (hold 35 min)</u>
~~Detector temperature~~:   ~~250^0C~~
~~Injector temperature~~:   ~~150^0C~~

6.3   For automated systems, connect the samples to the GC and begin the analytical process.

    <u>6.3.1   Samples may be injected manually by injecting an aliquot with a ground glass syringe.</u>

6.4   Introduce the sample into the carrier gas stream through the injection valve.

6.5   Each separated component exits from the column into the FID where a response is generated.

6.6   Concentrations of hydrocarbons are calculated using data acquisition/ processing software that uses calibration data from the NIST-traceable propane calibration standard.

6.7   For compounds having concentrations above the documented range of instrument linearity, a smaller aliquot must be taken (for manual systems, a smaller syringe or smaller loop; for automated systems, a smaller loop) or the sample must be diluted.

6.8   The peak integrations are corrected as necessary in the data system. Any misplaced baseline segments are corrected in the reconstructed chromatogram.

6.9   The peak identifications provided by the computer are checked and corrected if necessary.

6.10   Target compounds that coelute are reported as the major component, as determined by the analysis of several samples by GC/MS or other methods. An exception to this is m- and p-xylene, where GC/MS data and fuel profiles are used to determine the relative contribution of each component to the peak. This method was used to determine the m- and p-xylene MIR value given in Appendix 1.

6.11   The Alumina PLOT column is programmed to 200°C to assure all compounds are eluted before the next run.

7.   **CALCULATIONS**

7.1   The target hydrocarbon concentrations, in ppbC, are calculated by the data system using propane as an external standard.

$$\text{Concentration}_{sample}\ (\text{ppbC}) =\ \text{Peak Area}_{sample}\ \text{x}\ \ \text{Response Factor}$$

where the response factor (RF) is calculated during daily calibration by:

$$RF = \frac{\text{Concentration of NIST-traceable propane standard, ppbC}}{\text{Area of propane peak}}$$

8.   **QUALITY CONTROL**

8.1   Blank Run - A blank (pure nitrogen or helium) is run each analysis day. All target hydrocarbon concentrations from the blank analysis must be below the LOD before the analysis may proceed. As an alternative to a daily blank run, a daily partial blank check in tandem with a weekly blank run may be used. A partial blank check is defined as a check of the calibration standard run for contamination over all but the propane region of the chromatograph. The calibration standard must consist of only propane and make-up gas, with the concentration of all organic compounds except methane and propane below 2 percent of the propane standard concentration. The weekly blank run will provide a check on contamination in the propane region of the chromatograph.

8.1.1   If the blank shows a peak greater than the limit of detection (LOD) in the region of interest, the source of contamination must be investigated and remedied.

8.2   Calibration Run - The calibration standard is analyzed each analysis day to generate the response factor used to quantify the sample concentrations.

8.3   Control Standard Run - The quality control standard is analyzed at least once each analysis day. Measurements of all compounds specified in Section 5.6 must fall within the control limits to ensure the validity of the sample analyses that day. To meet this requirement, it may be necessary to inspect and repair the GC, and rerun the calibration and/or control standards.

8.4   Control Charts - A quality control chart is maintained for each component of the control standard listed in Section 5.6. The control charts, used on a daily basis, establish that the method is "in- control." The following describes how to construct a typical control chart:

1.   Obtain at least 20 daily control standard results;
2.   Calculate the control standard mean concentration and standard deviation for the target hydrocarbon; and
3.   Create a control chart for the target hydrocarbon by placing the concentration on the Y-axis and the date on the X-axis. Establish upper and lower warning limits at either two standard deviations (2s) or 5 percent, whichever is greater, above and below the average concentration. Establish upper and lower control limits at either three standard deviations (3s) or 5 percent, whichever is greater, above and below the average concentration.
4.   A control standard measurement is considered to be out-of-control when the analyzed value exceeds the control limit or two successive control standard measurements of the same analyte exceed the warning limit.
5.   If 20 control standard measurements are not yet available to create a control chart (e.g., the control standard was expended and replaced prior to obtaining 20 points with the new standard), measurements must be within 10% of the certified concentration. If the control standard is not a NIST standard, the cylinder should be certified by the laboratory against a NIST standard.

The measured concentrations of all target hydrocarbons contained in the control standard must be within the control limits (in-control) for the sample results to be considered acceptable.

8.5   Duplicates - A duplicate analysis of one sample is performed at least once per analysis day. The relative percent difference (RPD) is calculated for each duplicate run:

RPD (%) = $\dfrac{|\text{Difference between duplicate and original measurements}|}{\text{Average of duplicate and original measurements}} \times 100$

For each compound specified in Section 5.6, the allowable RPD depends on the average concentration level for the duplicate runs, as shown in the following table:

Average Measurement for the Duplicate Runs			Allowable RPD (%)
1 to 10	times	LOD	100
10 to 20	"	"	30
20 to 50	"	"	20
Greater than 50	"	"	15

If the results of the duplicate analyses do not meet these criteria for all compounds specified in Section 5.6, the sample may be reanalyzed. If reanalysis is not feasible or if the criteria are still not met on reanalysis, all sample results for that analysis day are invalid.

8.6   Linearity - A multipoint calibration to confirm instrument linearity is performed for the target hydrocarbons in the control standard for new instruments, after making instrument modifications that can affect linearity, and at least once every year unless a daily check of the instrument response indicates that the linearity has not changed. To monitor the instrument response, a quality control chart is constructed, as specified in Section 8.4, except using calibration standard area counts rather than control standard concentrations. When the standard area counts are out-of-control, corrective action(s) must be taken before analysis may proceed. The multipoint calibration consists of at least five concentration or mass loading levels (using smaller or larger volume sample sizes of existing standards is acceptable), each above the LOD, distributed over the range of expected sample concentration. Each concentration level is measured at least twice. A linear regression analysis is performed using concentration and average area counts to determine the regression correlation coefficient (r). The r must be greater than 0.995 to be considered sufficiently linear for one-point calibrations.

8.7   Limit of Detection – The LOD for the target hydrocarbons in the control standard must be determined ~~must be determined~~ for new instruments and after making instrument modifications that can affect linearity and/or sensitivity and at least once every year unless a daily check of the instrument response indicates that the LOD has not changed. To monitor the instrument response, a quality control chart is constructed, as specified in Section 8.4, except using calibration standard area counts rather than control standard concentrations. When the calibration standard area counts are out-of-control, investigation and/or corrective action(s) must be taken. To make the calculations, it is necessary to perform a multipoint calibration consisting of at least four "low" concentration levels, each above the LOD, with at least five replicate determinations of the lowest concentration

standard. A linear regression is performed and the standard deviation is converted to concentration units using the slope of the linear regression:

$$s = s_a \div m$$

where m is the slope of the linear regression, s is the standard deviation (in concentration units) of the lowest concentration standard and s_a is the standard deviation (in area counts) of the lowest concentration standard.

The LOD must be calculated using the following equation [Ref. 12]:

$$LOD = t * s$$

where s is the standard deviation (in concentration units) of at least five replicate determinations of the lowest concentration standard and t is the t-factor for 99 percent confidence for a one-sided normal (Gaussian) distribution. The number of degrees of freedom is equal to the number of replicates, minus one. An abbreviated t-table is:

Degrees of Freedom	t-value
4	3.7
5	3.4
6	3.1
7	3.0

The lowest standard must be of a concentration of one to five times the estimated LOD.

8.7.1   The maximum allowable LOD for each compound is 5 ppbC. The calculated laboratory LOD must be equal to or lower than the maximum allowable LOD. All peaks identified as target compounds that are equal to or exceed the maximum allowable LOD must be reported. If the calculated laboratory LOD is less than the maximum allowable LOD, the laboratory may choose to set its reporting limit at the maximum allowable LOD, the calculated laboratory LOD, or any level in between.

8.7.2   For the purpose of calculating the total mass of all species, the concentrations of all compounds below the LOD are considered to be zero.

8.8   Method No. 1002/Method No. 1003 Crossover Check - For each sample, a compound shall be measured by both Method No. 1002 and Method No. 1003. The crossover compound shall be a compound that can reasonably be expected to be found and measured by both methods in the laboratory performing the analysis. The results obtained by the two methods should be compared and an acceptance criteria set for the relative percent difference.

Part E

**DETERMINATION OF C$_6$ TO C$_{12}$ HYDROCARBONS
IN AUTOMOTIVE SOURCE SAMPLES BY GAS CHROMATOGRAPHY**

METHOD NO. 1003

1.   INTRODUCTION

1.1   This document describes a gas chromatographic method of ~~analyzing~~ measuring
         C$_6$ to C$_{12}$ hydrocarbons (mid-range hydrocarbons) in the ppbC range from
         automotive source samples. This method does not include sample collection
         procedures [Ref. 7]. The target hydrocarbons (compounds of interest) that shall
         be analyzed and reported by this method and Method 1002 are listed in Appendix
         1. All compounds on this list, when measured in concentrations above the LOD,
         shall be measured and reported ("targeted") by either Method 1002 or Method
         1003. Each laboratory should divide the list into light-end (Method 1002) and
         mid-range (Method 1003) hydrocarbons in the manner that best suits the
         laboratory instrumentation. All compounds on the list not targeted by Method
         1003 must be targeted by Method 1002.

1.2   Other applicable forms of instrumentation and analytical techniques may be used
         if shown to yield results equivalent to those specified in this procedure and if
         approved in advance by the Executive Officer of the Air Resources Board.

1.3   All definitions and abbreviations are contained in Appendix 2 of these test
         procedures.

2.   **METHOD SUMMARY**

2.1   This is a method intended for routine analysis.

2.2   The samples are received by the laboratory in ~~Tedlar~~ Kynar® bags, which are
         sub-sampled into a GC for separation and analysis.

2.3   The gas chromatographic analysis is performed through a temperature-
         programmed capillary column. A FID is used for detection.

2.4   The sample is injected into the GC by means of gas sampling valves. Separation
         of the sample hydrocarbon mixture into its components takes place in the
         chromatographic column. The chromatographic column and the corresponding
         operating parameters described in this method normally provide complete
         resolution of most target hydrocarbons.

2.5   The computerized GC data acquisition system identifies the hydrocarbons
         associated with each peak. The hydrocarbon concentrations are determined by

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integrating the peak areas and using a response factor determined from NIST-traceable standards.

3.   INTERFERENCES AND LIMITATIONS

3.1   An ~~interferent~~ interfering compound is any component present in the sample with a retention time similar to that of any target hydrocarbon described in this method. To reduce interference error, proof of chemical identity may require periodic confirmations using an alternate method and/or instrumentation, e.g., GC/MS, PID, different column, etc.

3.2   The concentration of hydrocarbons in the range of interest is stable for at least 24 hours in the Tedlar sampling bags, provided the sample bags do not leak and are not exposed to bright light or excessive heat. Sampling bags must be shielded from direct sunlight to avoid photochemically induced reactions of any reactive hydrocarbons. Samples must be analyzed within 24 hours.

4.   INSTRUMENTATION AND APPARATUS

4.1   ~~Tedlar~~ Kynar® (polyvinylidene fluoride) bags, ~~2~~ 4 mil in thickness, nominally 5 to 10 liters in capacity and equipped with quick-connect fittings, are typically used to contain the samples. Other sample collection containers, such as bags made of Tedlar® (polyvinyl fluoride) film or nickel-coated stainless steel canisters, may be used, provided they are made of non-reactive material and do not cause sample loss or contamination.

4.2   For manual sub-sampling into a GC, a ground glass syringe is used to transfer gaseous samples from Tedlar bags to the GC sample inlet. For automated systems, a sample loop is used to transfer gaseous samples from the Tedlar bag to the sample inlet of the GC. Sample aliquot size is chosen based on considerations of instrument sensitivity and/or linearity.

4.3   The GC is equipped with a FID, and a gas sampling valve system.

4.4   A non-polar capillary column [e.g., ~~J&W~~ Varian DB-1 (methylsiloxane), typically 60 m x 0.32 mm ID, film thickness 1.0 µ] is used. Other columns may be used, provided the alternate(s) can be demonstrated to the ARB to be equivalent or better with respect to precision, accuracy and resolution of all the target hydrocarbons.

4.5   A sample trap capable of being cryogenically cooled may be used.

4.6   A computer-controlled data acquisition system is required for quantifying peak areas.

5.   **REAGENTS AND MATERIALS**

5.1   Helium shall have a minimum purity of 99.995 percent. Higher purity helium may be required to achieve the LOD required by Section 8.7.1.

5.2   Hydrogen shall have a minimum purity of 99.995 percent.

5.3   Air shall be "Zero" grade (<1 ppmC total hydrocarbon contamination) or better.

5.4   Nitrogen shall have a minimum purity of 99.998 percent.

5.5   Calibration Standard - The quantitative calibration standard for all target hydrocarbons shall be propane at a concentration level between 0.25 and 1 ppm-mole and within the calculated linearity of the method. (See Section 8.6.) This propane standard must be a NIST-certified SRM or secondary NIST-traceable standard. A secondary standard is obtained by a comparison between a SRM and a candidate standard.

5.6   Control Standard - A quality control standard, containing at least n-hexane, n-octane, n-decane, benzene, toluene, and m- or p-xylene with concentrations between 0.2 and 1 ppmC based on a propane standard, is used for the following purposes:

    1.   Daily update of control charts, and
    2.   Daily determination of marker retention time windows.

5.7   A high concentration standard (higher than the calibration standard), containing the target hydrocarbons listed in Section 5.6, is used for linearity determinations. The high concentration standard must have concentrations verified against a NIST-traceable propane standard. (See Section 5.5 for the definition of NIST-traceable.) This verification can be performed at the laboratory performing the analysis.

5.8   A low concentration standard (one to five times the estimated LOD), containing the target hydrocarbons listed in Section 5.6, is used for LOD determinations. The low concentration standard must have concentrations verified against a NIST-traceable propane standard. (See Section 5.5 for the definition of NIST-traceable.) This verification can be performed at the laboratory performing the analysis.

    5.8.1   In lieu of a low concentration standard, a higher concentration standard may be diluted.

5.9   Liquid nitrogen may be required to cool the cryogenic trap and column oven where applicable.

6.   **PROCEDURE**

6.1   <u>The gaseous sample is analyzed for the target hydrocarbons C_5 through C_{12}.</u>

~~6.1   Typical operating conditions.~~

~~6.1.1   Suggested operating conditions for the manual GC are:~~
~~Helium carrier gas velocity: 30 cm/sec at 200°C~~
~~Nitrogen make-up gas flow: sufficient such that the total flow of helium plus nitrogen is 30 mL/min~~
~~Hydrogen gas flow (for FID):   30 mL/min~~
~~"Zero" air gas flow (for FID):   300 mL/min~~
~~Autozero FID at: 0.0 min~~
~~Range 11, Attenuation 8 (or another suitable value)~~
~~Sample valve temperature: 150°C~~
~~Injector temperature: 150°C~~
~~Column entrance port temperature: 95°C~~
~~Detector temperature: 250°C~~
~~Column temperature: Initial temperature 0°C; 10°C/min to 200°C~~

6.<u>2</u>~~.1.2~~   ~~Suggested~~ <u>Typical</u> operating conditions for the automated GC are:

Helium carrier gas flow <u>flow</u> ~~velocity~~:   ~~30 cm/sec~~ <u>2.2 mL/min</u> at 200°C
<u>Detector (0.010" FID)</u>
<u>Temperature:</u>   <u>275°C or higher</u>
Nitrogen make-up gas flow: sufficient such that the total flow of helium plus nitrogen is ~~30~~ <u>25</u> mL/min
Hydrogen gas flow (for FID):   ~~30~~ <u>25</u> mL/min
"Zero" air gas flow (for FID):   300 mL/min
Range 12, attenuation 8 (or another suitable value)
~~Sample~~ <u>Autosampler</u> valve temperature: 150°C
~~Detector temperature: 300°C~~
~~Injector temperature: 150°C~~
<u>Cryotrap temperature:</u>   <u>-180 °C (hold to trap hydrocabons)</u>
                                    <u>200 °C (heat to release hydrocarbons)</u>
<u>Analytical column valve oven temperature:</u>   <u>150°C</u>
Column temperature<u> program</u>:   <u>-40°C (hold 2.5 min)</u>
                                    <u>3.6°C/min to 210°C</u>
                                    <u>210°C (hold 5 min)</u>
                                    ~~Initial temperature -50°C (5 min),~~
                                    ~~5°C/min to 50°C,~~
                                    ~~10°C/min to 200°C~~

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6.2.1   Samples may be injected manually by injecting an aliquot with a ground glass syringe.

6.3   Data Reduction

6.3.1   The results are calculated from the FID responses.

6.3.2   The results are examined to see that the peaks are correctly integrated.

6.3.3   After running a particularly "dirty" sample, the analyst should run a blank before proceeding to the next sample as there may be sample carryover, or flush the sampling system with air.

6.3.4   The peak identifications provided by the computer are reviewed and, if necessary, corrected using the following procedure and criteria:

1.   The relative retention indices from GC/MS analyses are used to help confirm peak identifications.
2.   The primary peak identification is done by the computer using the relative retention times based on reference calibration runs.
3.   Confirm that the relative peak heights of the sample run ("fingerprint") match the typical fingerprint seen in past sample runs.
4.   Compare the relative retention times of the sample peaks with those of reference runs.
5.   Any peak with a reasonable doubt is labeled 'Unidentified'.

6.3.5   For compounds having concentrations above the documented range of instrument linearity, a smaller aliquot must be taken (for manual systems, a smaller syringe or smaller loop; for automated systems, a smaller loop) or the sample must be diluted.

6.3.6   The concentrations of the hydrocarbons are calculated using data acquisition/ processing software which uses calibration data from a NIST-traceable propane calibration standard.

6.3.7   Target compounds that coelute are reported as the major component, as determined by the analysis of several samples by GC/MS or other methods. An exception to this is m- and p-xylene, where GC/MS data and fuel profiles are used to determine the relative contribution of each component to the peak. This method was used to determine the m- and p-xylene MIR value given in Appendix 1.

7. **CALCULATIONS**

7.1   The target hydrocarbon concentrations, in ppbC, are calculated by the data system using propane as an external standard.

$$\text{Concentration}_{sample}\ (ppbC) = \text{Peak Area}_{sample}\ * \ \text{Response Factor}$$

where the Response Factor (RF) is calculated during daily calibration by:

$$RF = \frac{\text{Concentration of NIST} - \text{traceable propane standard, ppbC}}{\text{Area of propane peak}}$$

8. **QUALITY CONTROL**

8.1   Blank Run - A blank (pure nitrogen or helium) is run each analysis day. All target hydrocarbon concentrations from the blank analysis must be below the LOD before the analysis may proceed. As an alternative to a daily blank run, a daily partial blank check in tandem with a weekly blank run may be used. A partial blank check is defined as a check of the calibration standard run for contamination over all but the propane region of the chromatograph. The calibration standard must consist of only propane and make-up gas, with the concentration of all organic compounds except methane and propane below 2 percent of the propane standard concentration. The weekly blank run will provide a check on contamination in the propane region of the chromatograph.

      8.1.1   If the blank shows a peak greater than the limit of detection (LOD) in the region of interest, the source of the contamination must be investigated and remedied.

8.2   Calibration Run - The calibration standard is analyzed each analysis day to generate the response factor used to quantify the sample concentrations.

8.3   Control Standard Run - The quality control standard is analyzed at least once each analysis day. Measurements of all compounds specified in Section 5.6 must fall within the control limits to ensure the validity of the sample analyses that day. To meet this requirement, it may be necessary to inspect and repair the GC, and rerun the calibration and/or control standards.

8.4   Control Charts - A quality control chart is maintained for each component of the control standard listed in Section 5.6. The control charts, used on a daily basis, establish that the method is "in-control". The following describes how to construct a typical control chart:

      1.   Obtain at least 20 daily control standard results,
      2.   Calculate the control standard mean concentration and standard deviation for the target hydrocarbon, and

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3.   Create a control chart for the target hydrocarbon by placing the concentration on the Y-axis and the date on the X-axis. Establish upper and lower warning limits at either two standard deviations (2s) or 5 percent, whichever is greater, above and below the average concentration. Establish upper and lower control limits at either three standard deviations (3s) or 5 percent, whichever is greater, above and below the average concentration.

4.   A control standard measurement is considered to be out-of-control when the analyzed value exceeds the control limit or two successive control standard measurements of the same analyte exceed the warning limit.

5.   If 20 control standard measurements are not yet available to create a control chart (e.g., the control standard was expended and replaced prior to obtaining 20 points with the new standard), measurements must be within 10% of the certified concentration. If the control standard is not a NIST standard, the cylinder should be certified by the laboratory against a NIST standard.

The measured concentrations of all target hydrocarbons contained in the control standard must be within the control limits (in-control) for the sample results to be considered acceptable.

8.5   Duplicates - A duplicate analysis of one sample is performed at least once per analysis day. The relative percent difference (RPD) is calculated for each duplicate run:

$$RPD(\%) = \frac{|\text{ Difference between duplicate and original measurements }|}{\text{Average of duplicate and original measurements}} * 100$$

For each compound specified in Section 5.6, the allowable RPD depends on the average concentration level for the duplicate runs, as shown in the following table:

Average Measurement for Duplicate Runs			Allowable RPD (%)
1 to 10	times	LOD	100
10 to 20	"	"	30
20 to 50	"	"	20
Greater than 50	"	"	15

If the results of the duplicate analyses do not meet these criteria for all compounds specified in Section 5.6, the sample may be reanalyzed. If reanalysis is not feasible or if the criteria are still not met on reanalysis, all sample results for that analysis day are invalid.

8.6   Linearity - A multipoint calibration to confirm instrument linearity is performed for all target hydrocarbons in the control standard for new instruments, after making instrument modifications that can affect linearity, and at least once every

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year unless a daily check of the instrument response indicates that the linearity has not changed. To monitor the instrument response, a quality control chart is constructed, as specified in Section 8.4, except using calibration standard area counts rather than control standard concentrations. When the standard area counts are out-of-control, corrective action(s) must be taken before analysis may proceed. The multipoint calibration consists of at least five concentration or mass loading levels (using smaller or larger volume sample sizes of existing standards is acceptable), each above the LOD, distributed over the range of expected sample concentration. Each concentration level is measured at least twice. A linear regression analysis is performed using concentration and average area counts to determine the regression correlation coefficient (r). The r must be greater than 0.995 to be considered sufficiently linear for one point calibrations.

8.7   Limit of Detection - The LOD for the target hydrocarbons in the control standard must be determined for new instruments and after making instrument modifications that can affect linearity and/or sensitivity and at least once every year unless a daily check of the instrument response indicates that the LOD has not changed. To monitor the instrument response, a quality control chart is constructed, as specified in Section 8.4, except using calibration standard area counts rather than control standard concentrations. When the calibration standard area counts are out-of-control, investigation and/or corrective action(s) must be taken. To make the calculations, it is necessary to perform a multipoint calibration consisting of at least four "low" concentration levels, each above the LOD, with at least five replicate determinations of the lowest concentration standard. A linear regression is performed and the standard deviation (in area counts) of the lowest concentration standard determined. The standard deviation is converted to concentration units using the slope of the linear regression:

$$s = \ s_a \div m$$

where m is the slope of the linear regression, s is the standard deviation (in concentration units) of the lowest concentration standard and s_a is the standard deviation (in area counts) of the lowest concentration standard.

The LOD must be calculated using the following equation [Ref. 12]:

$$LOD = t * s$$

where s is the standard deviation (in concentration units) of at least five replicate determinations of the lowest concentration standard and t is the t-factor for 99 percent confidence for a one-sided normal (Gaussian) distribution. The number of degrees of freedom is equal to the number of replicates, minus one. An abbreviated t-table is:

Degrees of Freedom	t-value
4	3.7
5	3.4
6	3.1
7	3.0

The lowest standard must be of a concentration of one to five times the estimated LOD.

8.7.1   The maximum allowable LOD for each compound is 5 ppbC. The calculated laboratory LOD must be equal to or lower than the maximum allowable LOD. All peaks identified as target compounds that are equal to or exceed the maximum LOD must be reported. If the calculated laboratory LOD is less than the maximum allowable LOD, the laboratory may choose to set its reporting limit at the maximum allowable LOD, the calculated laboratory LOD, or any level in between.

8.7.2.   For the purpose of calculating the total mass of all species, the concentrations of all compounds below the LOD are considered to be zero.

8.8   Method No. 1002/Method No. 1003 Crossover Check - For each sample a compound shall be measured by both Method No. 1002 and Method No. 1003. The crossover compound shall be a compound that can reasonably be expected to be found and measured by both methods in the laboratory performing the analysis. The results of the two analyses should be compared and an acceptance criteria set for the relative percent difference.

Part F

**DETERMINATION OF ALDEHYDE AND KETONE COMPOUNDS
IN AUTOMOTIVE SOURCE SAMPLES
BY HIGH PERFORMANCE LIQUID CHROMATOGRAPHY**

METHOD NO. 1004

1.   **INTRODUCTION**

1.1   This document describes a method of analyzing automotive source samples engine exhaust for aldehyde and ketone compounds (carbonyls) using impingers, containing acidified 2,4-dinitrophenylhydrazine (DNPH) absorbing solution, or DNPH-impregnated cartridges. Carbonyl masses ranging between 0.02 to 200 µg are measured by this method. The "target" carbonyls (compounds of interest) that shall be analyzed measured and reported by this method are listed in Appendix 1. All of these carbonyl compounds, when measured in concentrations above the LOD, shall be reported.

    1.1.1   For the purpose of calculating NMOG for vehicles tested on exhaust emission test fuel containing ethanol (see Part G, Determination of NMOG Mass Emissions):

    1.1.1.1   The only carbonyl compounds that need to be reported from this method are formaldehyde and acetaldehyde.

    1.1.1.2   The additional carbonyls listed in Appendix 1 are within the scope of this analytical method and their measurement may provide meaningful information to the laboratory. However, their measurement is not required.

1.2   This procedure is derived from a method used by Hull [Ref. 10].

1.3   Other applicable forms of instrumentation and analytical techniques may be used if shown to yield results equivalent to those specified in this procedure and if approved in advance by the Executive Officer of the Air Resources Board.

1.4   All definitions and abbreviations are contained in Appendix 2 of these test procedures.

2.   **METHOD SUMMARY**

2.1   The samples are received by the laboratory in sample collection cartridges or impingers. (See Section 4.2.) The DNPH reagent absorbing solution (2,4 DNPH)

complexes the carbonyl compounds into their diphenylhydrazone derivatives. The cartridges are then <u>extracted</u> ~~eluted~~ with ~~5 mL~~ acetonitrile.

2.2   Separation and analysis are performed using a HPLC with an ultraviolet detector.

3.   INTERFERENCES AND LIMITATIONS

3.1   An ~~interferent~~ <u>interfering compound</u> is any detectable compound present in the sample with a retention time very similar to that of any target carbonyl described in this method. To reduce interference error, proof of chemical identity may require periodic confirmations using an alternate method and/or instrumentation, e.g., alternative HPLC columns or mobile phase compositions.

3.2   If samples are not analyzed the same day as received, they must be refrigerated at a temperature below 40^oF.

       3.2.1   <u>Impinger solutions must first be transferred to glass bottles and sealed.</u> ~~Refrigerated samples are stable for up to 30 days.~~

       3.2.2   <u>If cartridges are not immediately extracted they must be refrigerated.</u>

       3.2.3   <u>Acrolein and crotonaldehyde have been shown to degrade in acidified DNPH cartridges; hence, it is recommended to extract the cartridges as soon as possible. The extract must be refrigerated.</u>

       3.2.4   <u>Refrigerated cartridge sample extracts and impinger solutions are stable for up to 30 days.</u>

~~3.3   When using the DuPont Zorbax or Supelco's Supelcosil columns described in Section 4.1.5, methyl ethyl ketone (MEK) and butyraldehyde tend to coelute.~~

~~3.4   When using the Delta Bond column described in Section 4.1.5, formaldehyde tends to coelute with an unknown, non-carbonyl compound, and the tolualdehyde isomers tend to coelute. The guard column for the Delta Bond column must also be changed frequently in order to prevent the coelution of butyraldehyde and methacrolein and to prolong the life of the column.~~

3.3   <u>The presence of NOx in exhaust samples depletes DNPH in the cartridges. Laboratories should develop criteria to validate test results by ensuring that enough DNPH is left to trap the carbonyl compounds.</u>

4.   INSTRUMENT AND APPARATUS

4.1   The HPLC analytical system consists of the following:

       4.1.1   Dual high pressure pumps.

4.1.2　Automated gradient controller or pump module controller.
4.1.3　Temperature controller module for the column oven.
4.1.4　A liquid autosampler.
4.1.5　The ~~primary~~ system incorporates two ~~DuPont Zorbax ODS or Supelco's Supelcosil~~ LC-18 columns (e.g., Supelco's Supelcosil, typically 25cm x 4.6mm, 5μ silica gel particles) in tandem and a guard column (e.g., Supelco's Pelliguard, 2 cm long packed with LC18 5 μm pellicular beads). ~~The secondary system incorporates a Delta Bond AK (4.6 mm ID x 200 mm) packed column with a guard column 2 cm long packed with LC18 5 μm pellicular beads or equivalent).~~ Other columns may be used, provided the alternate(s) can be demonstrated to the ARB to be equivalent or better with respect to precision, accuracy and resolution of all target carbonyls.

4.1.6　An ultraviolet/visible (UV/VIS) detector.
4.1.7　Data system for peak integration.

4.2　Samples are collected ~~collection containers~~ ~~are~~ in glass impingers or DNPH-impregnated cartridges.

5.　REAGENTS AND MATERIALS

5.1　Acetonitrile, HPLC grade~~,~~ (Burdick and Jackson or equivalent).

5.2　Water, HPLC grade~~,~~ (Burdick and Jackson or equivalent).

5.3　Methanol, HPLC grade (Burdick and Jackson or equivalent).

5.4　Acidified DNPH-Silica cartridges (Waters Corp. or equivalent).

5.5~~3~~　~~2,4-~~DNPH, purified, Radian Corporation or equivalent. Unpurified DNPH must be recrystallized twice from acetonitrile. The recrystallized DNPH is checked for contaminants by injecting a dilute solution of DNPH in contaminant-free acetonitrile into the HPLC.

5.6~~4~~　Sulfuric acid, or perchloric acid, analytical reagent grade~~,~~ (Baker Analyzed or equivalent).

5.7~~5~~　The carbonyl/~~2,4-dinitrophenylhydrazone (DNPH)~~ complexes [Ref. 11] listed in Table F1 may be purchased (e.g., Radian Corporation, in 1.2 mL ampules) or prepared in the laboratory. In-house standards must be recrystallized at least three times from 95 percent ethanol.

TABLE F-1
PROPERTIES OF CARBONYL/2,4-DNPH COMPLEXES

Complex	Molecular Weight (g/mole)	Melting Point ^{o}C
formaldehyde	210.15	165-166
acetaldehyde	224.18	152-153
acrolein	236.19	165[1]
acetone	238.20	125-127
propionaldehyde	238.20	144-145
butyraldehyde	252.23	119-120
hexanaldehyde	280.28	106-107
benzaldehyde	286.25	240-242
methyl ethyl ketone	252.53	117-118
methacrolein	250.21	200-201
crotonaldehyde	250.21	185-188
valeraldehyde	266.26	107-108
m-tolualdehyde	300.27	212

5.86 Stock Calibration Standard - A stock calibration standard is prepared by diluting the target carbonyl/2,4-DNPH complexes with acetonitrile. A typical stock calibration standard contains 3.0 µg/mL of each target carbonyl compound. Stock calibration standards of other concentrations may also be used.

5.97 Working Standard - A working standard is prepared when required by diluting the stock calibration solution, making sure that the highest concentration of the standard is above the expected test level. Typically, the 3.0 µg/mL stock is diluted five times with acetonitrile in a volumetric flask to yield a 0.6 µg/mL solution.

5.108 Control Standard - A quality control standard, containing all target carbonyls/2,4-DNPH complexes within the typical concentration range of real samples, is analyzed to monitor the precision of the analysis of each target carbonyl. The control standard may be purchased, prepared in the laboratory from a stock solution different from the calibration standard, or prepared by batch mixing old samples, spiking it with a stock solution of target compounds, and stirring for a minimum of 2 hours. If necessary, the solution is filtered using filter paper to remove precipitation. All target compounds except acrolein have been found to be stable in the control standard.

5.119 Standards used for linearity and LOD determinations (Section 8) may be purchased or prepared by dilutions of an appropriate level stock solution.

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[1]This compound has been known shown to decompose.

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6. **PROCEDURE**

6.1   For systems collecting the samples via impingers, an absorbing solution is
        prepared by dissolving 0.11 - 0.13 grams of recrystallized DNPH in 1 L of HPLC
        grade acetonitrile. The absorbing solution should be prepared at least every two
        weeks. Each batch of acetonitrile used in this procedure is checked for
        oxygenated impurities by adding it to a contaminant-free dilute solution of DNPH
        and analyzing by HPLC.

    6.1.1   In the laboratory, pipette 15 mL of the DNPH absorbing solution into each
            of the 30 mL impingers for each emission test. Add 0.1 mL of 2.85 N
            sulfuric acid or 0.15 mL of 3.8 M perchloric acid to each impinger.

6.2   For systems collecting the samples via cartridges, DNPH-impregnated cartridges
        shall be sealed and refrigerated, at a temperature less than 40°F, upon receipt from
        manufacturer, until ready for use.

    6.2.1   At the exhaust volumes being sampled (1 L/min), a back-up cartridge may
            be required for CVS phase 1 or other high-concentration sample but no
            back-up cartridge is needed for CVS phases 2 and 3 or other low-
            concentration samples.

6.3   After sampling uncap and place all impingers in preheated water at 70-80°C for
        30 minutes (min) to complete derivatization. Heating is not required when using
        perchloric acid.

    6.3.1   For cartridges, remove the caps and extract with 5 mL acetonitrile,
            running the extract into glass storage bottles.

6.4   Remove the impingers from the water bath and cool to room temperature.
        Replace any lost solvent by adding acetonitrile to the 15-mL mark.

    6.4.1   Replacing lost solvent is not required when using an internal standard
            method (Section 7.4).

6.5   Transfer the solution from each impinger/cartridge to glass vials and seal with
        new septum screw caps.

6.6   Place the vials containing blank, working standard, control standard, and samples
        into the autosampler for subsequent injection into an HPLC. Suggested standard
        operating conditions for the HPLC are:

        ~~Primary~~ Typical System:
        Columns: ~~4.6 mm ID x 250 mm x 1/4 inches OD Dupont Zorbax~~
                                ~~ODS or~~ Supelco Supelcosil (LC-18, 25cm x 4.6mm, 5µm
                                silica gel particles), –two columns in series, and a Supelco

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Pelliguard ~~G~~guard column~~—~~ (2 cm long packed with C18
5 µm pellicular beads)

Column temperature: 40°C
Detector: UV/VIS at 360 nm
Sample volume: 10 µL
Solvent A: acetonitrile
Solvent B: ~~10 percent (volume/volume)~~ methanol ~~in water~~
Solvent C: water
Flow: 1.2 mL/min
Program:

50 percent A, 5~~0~~ percent B, 45 percent C   0 (initial time)
65 percent A, 3.5 percent B, 31.5 percent C 0 to 30 ~~2~~ min (linear ramp)
100 percent A, 0 percent B, 0 percent C   ~~2~~ 30 to 40 ~~22~~ min (linear ramp)
100 percent A, 0 percent B, 0 percent C   40 to 42 min (hold)
50 percent A, 5~~0~~ percent B, 45 percent C   ~~22~~ 42 to 45 ~~37~~ min (linear ramp)

~~Under the above configuration, methyl ethyl ketone and butyraldehyde tend to coelute. In order to report these compounds, it is necessary to analyze the samples using a secondary system. The tolualdehyde isomers (m-, p-, and o-) are separated using this configuration. The reporting of tolualdehyde is addressed in Section 7.4.~~

~~Secondary System:~~
~~Columns: Delta Bond AK C18 (4.6 mm ID x 200 mm x 1/4 in OD) packed column, Guard column - 2 cm long packed with C18 5 µm pellicular~~
~~Column temperature: 40°C~~
~~Detector: UV/VIS at 360 nm~~
~~Sample volume: 10 µL~~
~~Solvent A: acetonitrile~~
~~Solvent B: acetonitrile in water, 35 percent (v/v)~~
~~Flow: 1.5 mL/min~~
~~Program: 0 percent A, 100 percent B   0 (initial time)~~
~~23 percent A, 77 percent B   0 - 5.5 min~~
~~46 percent A, 54 percent B   5.5 - 13 min~~
~~0 percent A, 100 percent B   13 to 30 min~~

~~This secondary system is not used to report all compounds because formaldehyde tends to coelute with a non-carbonyl compound. If this coelution is resolved, the secondary system may be used alone to analyze all carbonyl compounds. The tolualdehyde isomers, however, are not separated with this configuration. The reporting of tolualdehyde is addressed in Section 7.4.~~

Data System: The outputs from the UV/VIS detector are sent to a PC-controlled data acquisition system.

6.7   If all target compounds are not separated using this configuration, a second HPLC
        with a different configuration must be used, in addition to the primary system, to
        separate the coeluting compounds.

6.8~~7~~   The peak integrations are corrected as necessary in the data system. Any
        misplaced baseline segments are corrected in the reconstructed chromatogram.

6.9~~8~~   Samples containing compounds having concentrations above the documented
        range of instrument linearity must be diluted and reanalyzed.

7.   **CALCULATIONS**

7.1   For each target carbonyl, the carbonyl mass is calculated from its
        carbonyl/~~2,4~~ DNPH mass.

7.2   The mass of each carbonyl compound, per impinger or cartridge, is determined by
        the following calculation:

$$\text{Mass}_{\text{sample}} = \text{Peak Area}_{\text{sample}} * \text{Response Factor} * \text{Impinger}(\text{or Cartridge}) \text{ volume}(\text{mL}) * B$$

        where B is the ratio of the molecular weight of the carbonyl compound to its
        2,4-dinitrophenylhydrazone derivative and where the response factor (RF) for
        each carbonyl is calculated during the calibration by:

$$RF = \frac{\text{Concentration}_{\text{standard}} \ (\mu g \ \text{~~2,4~~ DNPH species/mL})}{\text{Peak Area}_{\text{standard}}}$$

7.3   For tolualdehyde, the sum of all isomers present is reported as m-tolualdehyde.

        7.3.1 ~~Under the conditions of the primary system in Section 6.6, the isomers are
               separated. The m-tolualdehyde response factor is applied to each peak and
               the sum reported as m-tolualdehyde.~~

        7.3.2 Under the conditions of the ~~secondary~~ system described in Section 6.6, the
               isomers coelute. The m-tolualdehyde response factor is applied to the
               single tolualdehyde peak. This concentration is reported as m-
               tolualdehyde.

7.4   An internal standard method may also be used.

8.   **QUALITY CONTROL**

8.1   Blank Runs

        8.1.1 Reagent Blanks - The solvents used are of the highest HPLC grade and are
               tested for impurities when a new lot number is used. If this lot number is

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found to be acceptable, (no carbonyls present at concentrations at or above the LOD), daily blank analysis is not performed.

8.1.2 Carbonyl/~~2,4~~-DNPH Purity - The carbonyl/~~2,4~~-DNPHs are checked for purity by their melting points and their chromatograms (See Table F-1). Analysis of the solution of carbonyl/~~2,4~~-DNPH must yield only the peak of interest. No contaminant peaks above the LOD should be observed.

8.1.3 Field Blanks – One cartridge is analyzed as a field blank for each emission test. If the field blank shows a peak greater than the limit of detection (LOD) in the region of interest, the source of the contamination must be investigated and remedied.

8.1.4 Cartridge Blanks - At least one cartridge per batch is analyzed as a batch blank. If the cartridge blank shows a peak greater than the limit of detection (LOD) in the region of interest, the source of the contamination must be investigated and remedied.

8.2 Calibration Run - The calibration standard is analyzed each analysis day to generate the response factors used to quantify the sample concentrations.

8.3 Control Standard Run - The quality control standard is analyzed at least once each analysis day. Measurements of all target compounds in the control standard, except acrolein, must fall within the control limits to ensure the validity of the sample analyses that day. To meet this requirement, it may be necessary to rerun the calibration and control standards, and inspect and repair the HPLC.

8.4 Control Charts - A quality control chart is maintained for each component of the control standard. The control charts, used on a daily basis, establish that the method is "in- control." The following describes how to construct a typical control chart:

1. Obtain at least 20 daily control standard results,
2. Calculate the control standard mean concentration, and standard deviation(s) for the target analyte, and
3. Create a control chart for the target analyte by placing the concentration on the Y-axis and the date on the X-axis. Establish an upper warning limit and a lower warning limit at two standard deviations (2s) above and below the average concentration. Establish an upper control limit and a lower control limit at three standard deviations (3s) above and below the average concentration.
4. Due to the low variability of the carbonyl control standard measurements, a control standard measurement is considered to be out-of-control when the analyzed value exceeds either the 3s limit, or the range of ± 10% of the mean control measurement, whichever is greater, or if two successive control standard measurements of the same analyte exceed the 2s limit.

5.   If 20 control standard measurements are not yet available to create a control chart (e.g., the control standard was expended and replaced prior to obtaining 20 points with the new standard), measurements must be within 10% of the assay (purchased) or theoretical (prepared in-house) concentration.

The measured concentrations of all target analytes contained in the control standard must be within the control limits (in-control) for the sample results to be considered acceptable. No control requirements have been established for acrolein, since it has been shown to degrade over time.

8.5   Duplicates - A duplicate analysis of one sample is performed at least once per analysis day. The relative percent difference (RPD) is calculated for each duplicate run:

$$RPD(\%) = \frac{|\text{ Difference between duplicate and original measurements }|}{\text{Average of duplicate and original measurements}} * 100$$

For each compound, the allowable RPD depends on the average concentration level for the duplicate runs, as shown in the following table:

Average Measurement for Duplicate Runs		Allowable RPD (%)
1 to 10	times LOD	100
10 to 20	" "	30
20 to 50	" "	20
Greater than 50	" "	15

If the results of the duplicate analyses do not meet these criteria for all target carbonyls, the sample may be reanalyzed. If reanalysis is not feasible or if the criteria are still not met on reanalysis, all sample results for that analysis day are invalid.

8.6   Linearity - A multipoint calibration to confirm instrument linearity is performed for all target analytes for new instruments, after making instrument modifications that can affect linearity, and at least once every year. The multipoint calibration consists of at least five concentration or mass loading levels (using smaller or larger volume sample sizes of existing standards is acceptable), each above the LOD, distributed over the range of expected sample concentration. Each concentration level is measured at least twice. A linear regression analysis is performed using concentration and average area counts to determine regression correlation coefficient (r). The r must be greater than 0.995 to be considered linear for one point calibrations.

8.7   Limit of Detection - The LOD for the target analytes must be determined for new instruments, after making instrument modifications which can affect the LOD and at least once per year. To make the calculations, it is necessary to perform a

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multipoint calibration consisting of at least four "low" concentration levels, each above the LOD, with at least five replicate determinations of the lowest concentration standard. A linear regression is performed and the standard deviation (in area counts) of the lowest concentration standard determined. The standard deviation is converted to concentration units using the slope of the linear regression:

$$s = s_a \div m$$

where m is the slope of the linear regression, s is the standard deviation (in concentration units) of the lowest concentration standard and s_a is the standard deviation (in area counts) of the lowest concentration standard.

The LOD must be calculated using the following equation [Ref. 12]:

$$LOD = t * s$$

where s is the standard deviation (in concentration units) of at least five replicate determinations of the lowest concentration standard and t is the t-factor for 99 percent confidence for a one-sided normal (Gaussian) distribution. The number of degrees of freedom is equal to the number of replicates, minus one. An abbreviated t-table is:

Degrees of Freedom	t-value
4	3.7
5	3.4
6	3.1
7	3.0

The lowest standard must be of a concentration of one to five times the estimated LOD.

8.7.1   The maximum allowable LOD is 0.0075 µg/mL. The calculated laboratory LOD must be equal to or lower than the maximum allowable LOD. All peaks identified as target compounds that are equal to or exceed the maximum allowable LOD must be reported. If the calculated laboratory LOD is less than the maximum allowable LOD, the laboratory may choose to set its reporting limit at the maximum allowable LOD, the calculated laboratory LOD, or any level in between.

8.7.2   For the purpose of calculating the total mass of all species, the concentrations of the compounds below the LOD are considered to be zero.

Part G
DETERMINATION OF NMOG MASS EMISSIONS

1. **INTRODUCTION**

1.1   NMOG mass emissions consist of non-methane hydrocarbons and oxygenated hydrocarbons.

1.2   All definitions and abbreviations are set forth in Appendix 2 of these test procedures.

2. **NMOG WEIGHTED MASS EMISSIONS**

2.1   ~~NMOG weighted mass (wm) emissions shall be calculated as follows:~~

$$\cancel{NMOG_{wm} = \sum NMHC_{wm} + \sum ROH_{wm} + \sum RHO_{wm}}$$

Non-methane hydrocarbon weighted mass emissions ($NMHC_{wm}$) can be determined by either ~~(~~FID or GC. If the FID method is used to calculate $NMHC_{wm}$, refer to Part B of these test procedures entitled, "Determination of Non-Methane Hydrocarbon Mass Emissions by Flame Ionization Detection." If the GC method is used to calculate $NMHC_{wm}$, refer to section 4~~3~~, "Speciated Hydrocarbon Mass Emissions Calculation," contained herein. Carbonyl weighted mass emissions (RHO_{wm}) are to be calculated according to section 6~~5~~, "Carbonyl Mass Emissions Calculation," contained herein. For alcohol fueled vehicles, alcohol weighted mass emissions (ROH_{wm}) are to be calculated according to section 5~~4~~, "Alcohol Mass Emissions Calculation," contained herein. Dilution factors and mass emission are determined according to section 3, "Dilution Factors and Mass Emission Calculation," contained herein.

If the FID method is used to determine the non-methane hydrocarbon weighted mass emissions, the NMHC sample measurement includes contributions from any oxygenated hydrocarbons that may be present in the sample. Therefore, the FID NMHC measurement must be corrected for the presence of alcohols and carbonyl compounds, to give a resultant value called non-oxygenated non-methane hydrocarbons (NONMHC). This correction may take place at the concentration level, for each sample and ambient background, or at the mass level, after $NMHC_{mass}$ and $NMHC_{wm}$ have been calculated. (The two operations are mathematically equivalent.) For the calculations presented in this document, the oxygenate correction is presumed to take place after $NMHC_{mass}$ and $NMHC_{wm}$ have been calculated.

2.2   NMOG weighted mass (wm) emissions, using the FID method, shall be calculated as follows:

$$\left(\text{NMOG}_{\text{wm}}\right)_{\text{FID}} = \sum \text{NONMHC}_{\text{wm}} + \sum \text{ROH}_{\text{wm}} + \sum \text{RHO}_{\text{wm}}$$

NONMHC$_{\text{wm}}$ is calculated according to the following equations:

$$\text{NONMHC}_{\text{wm}} = 0.43 * \left(\frac{\text{NONMHC}_{\text{mass1}} + \text{NONMHC}_{\text{mass2}}}{D_{\text{phase1}} + D_{\text{phase2}}} \right) + 0.57 * \left(\frac{\text{NONMHC}_{\text{mass3}} + \text{NONMHC}_{\text{mass2}}}{D_{\text{phase3}} + D_{\text{phase2}}} \right)$$

and

$$\text{NONMHC}_{\text{mass n}} = \text{NMHC}_{\text{mass n}} - \text{NMHC}_{\text{dens}} * \sum \left(\frac{\text{ROH}_{\text{mass n}}}{\text{ROH}_{\text{dens}}} \right) * r_{\text{ROH}} - \text{NMHC}_{\text{dens}} * \sum \left(\frac{\text{RHO}_{\text{mass n}}}{\text{RHO}_{\text{dens}}} \right) * r_{\text{RHO}}$$

where:

NMHC$_{\text{mass n}}$ = NMHC$_{\text{conc}}$ * NMHC$_{\text{dens}}$

2.3   NMOG weighted mass (wm) emissions, using the GC method, shall be calculated as follows:

$$\left(\text{NMOG}_{\text{wm}}\right)_{\text{GC}} = \sum \text{HC}_{\text{wm}} + \sum \text{ROH}_{\text{wm}} + \sum \text{RHO}_{\text{wm}}$$

In the GC method, the hydrocarbons are each measured individually and, therefore, the sum of species ($\sum$HC) does not include methane or oxygenated compounds. Thus, this method does not need the corrections that the FID method requires.

3.   **DILUTION FACTOR AND NMHC MASS EMISSION CALCULATION**

3.1   As shown in Part B, the dilution factor is determined using only the major constituents of the emission sample. The dilution factor is determined using the following equation:

$$\text{DF} = \frac{100 * \left(\dfrac{x}{x + y/2 + 3.76 * \left(x + y/4 - z/2 \right)} \right)}{\text{CO}_{2\text{e}} + \left(\text{NMHC}_{\text{e}} + \text{CH}_{4\text{e}} + \text{CO}_{\text{e}} \right) * 10^{-4}}$$

(where fuel composition is $C_xH_yO_z$ as measured for the fuel used; this expression is generally normalized so that $x = 1$)

3.2   The density of the NMHC is determined using the carbon:hydrogen ratio of the fuel, $C_xH_yO_z$, according to the following equation:

$$NMHC_{dens} = (x * 12.01115 + y * 1.00797)(g/mole) * \left(\frac{28.316847 \text{liter/ft3}}{24.0547 \text{liter/mole}} \right)$$

where: 12.01115 = atomic weight of carbon
1.00797 = atomic weight of hydrogen

a) For gasoline, $CH_{1.85}$, where x = 1, y = 1.85, and z = 0:
DF = 13.47 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]
$NMHC_{dens}$ = 16.33

b) For Phase 2 gasoline, $CH_{1.94}O_{0.017}$, where x = 1, y = 1.94 and z = 0.017,
DF = 13.295 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]
$NMHC_{dens}$ = 16.44

c) For LPG, $CH_{2.64}$, where x = 1, y = 2.64, z = 0:
DF = 11.68 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]
$NMHC_{dens}$ = 17.27

d) For CNG, $CH_{3.78}O_{0.016}$, where x = 1, y = 3.78, and z = 0.016:
DF = 9.83 / [[CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]
$NMHC_{dens}$ = 18.63

e) For E85, $CH_{2.7841}O_{0.3835}$, Where x = 1, y = 2.7841, and z = 0.3835:
DF = 12.4253 / [CO_{2e} + ($NMHC_e$ + CH_{4e} + CO_e) * 10^{-4}]
$NMHC_{dens}$ = 17.44

3.3   Sample Calculation

A flex-fuel vehicle using E85 fuel $CH_{2.7841}O_{0.3835}$, where x = 1, y = 2.7841, and z = 0.3835:

Test Phase	FID THC_e (ppmC)	CH_{4e} (ppmC)	CO_{2e} (%)	CO_e (ppm)	FID THC_d (ppmC)	CH_{4d} (ppmC)	CO_{2d} (%)	CO_d (ppm)	VMIX (ft^3)	$D_{phase\ n}$ (mile)
1	27.230	6.918	0.8564	117.801	3.532	2.261	0.0438	0.5224	3495	3.591
2	3.5459	2.357	0.5595	10.8229	3.476	2.247	0.4446	0.3322	5799	3.846
3	3.8510	2.590	0.7163	5.1538	3.396	2.188	0.4507	0.6752	3484	3.591

FID response factor of methane is experimentally determined for each individual FID. The value of 1.15 used here is for example only.

For phase 1:

$NMHC_e$ = FID THC_e – r_{CH_4} * CH_{4e}

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$$= 27.230 - 1.15 * 6.918$$
$$= 19.274 \text{ ppmC}$$

$$DF = 12.4253 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}]$$
$$= 12.4253 / [0.8564 + (19.274 + 6.918 + 117.801) * 10^{-4}]$$
$$= 14.2688 \text{ ppmC}$$

$$NMHC_d = FID\ THC_d - r_{CH_4} * CH_{4d}$$
$$= 3.532 - 1.15 * 2.261$$
$$= 0.9319 \text{ ppmC}$$

$$NMHC_{conc} = NMHC_e - NMHC_{d*} (1 - 1/DF)$$
$$= 19.274 - 0.9319 * (1 - 1 / 14.2688)$$
$$= 18.407 \text{ ppmC}$$

$$NMHC_{mass1} = NMHC_{conc} * NMHC_{dens} * VMIX_1 * 10^{-6}$$

$$= 18.407 * 17.44 * 3495 * 10^{-6}$$
$$= 1.1220 \text{ g}$$

Similarly, for Phase 2, $DF = 22.152$ and $NMHC_{mass2} = 0$

Similarly, for Phase 3, $DF = 17.332$ and $NMHC_{mass2} = 0.0026 \text{ g}$

34. SPECIATED HYDROCARBON MASS EMISSIONS CALCULATION

34.1 INTRODUCTION

Vehicular exhaust emissions are measured according to the FTP [Ref. 1]. For each of the three phases of the FTP, a ~~tedlar~~ sample collection bag, ~~of 0.5 ft³~~ nominally 5 to 10 liters in capacity, is used to collect a dilute exhaust sample. Sample collection bags may be made of Tedlar® (polyvinylfloride, or PVF), 2 mil in thickness, or of Kynar® or Solef® (polyvinylidenefloride, or PVDF), each 4 mil in thickness. A fourth ~~0.5 ft³~~ ~~tedlar~~ bag is used to collect a composite dilution air (background) sample from all three phases of the FTP. Since PVF and PVDF films contain plasticizer or volatile organic components, all of the films are conditioned in a vented oven at 250°F for 16 hours before made into sample bags. All bag samples are analyzed according to Method No. 1002 (Part D of these test procedures) and Method No. 1003 (Part E of these test procedures) to determine the dilute exhaust and dilution air concentrations of individual hydrocarbon compounds. The measured hydrocarbon compound concentrations are used in the following equations to calculate the weighted mass emissions of each hydrocarbon compound.

34.2 HC MASS EMISSIONS CALCULATION PER TEST PHASE

34.2.1 $HC_{mass\ n} = (HC_{conc} * HC_{dens} * VMIX * 10^{-6}) / (Carbon\ No.)$

34.2.2 $HC_{conc} = HC_e - (HC_d * (1 - (1 / DF)))$

   NOTE: If HC_{conc} is calculated to be less than zero, then $HC_{conc} = 0$.

34.3. WEIGHTED HC MASS EMISSIONS CALCULATION

34.3.1 $HC_{wm} = 0.43 * \left(\dfrac{HC_{mass1} + HC_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\dfrac{HC_{mass3} + HC_{mass2}}{D_{phase3} + D_{phase2}} \right)$

34.4. SAMPLE CALCULATION

34.4.1 Exhaust emissions from a gasoline vehicle are collected in three dilute exhaust sample bags and one dilution air (background) sample bag during the FTP. Gas chromatography is used to determine the benzene concentration of each bag sample. Calculate the weighted benzene mass emissions based on the following data:

Test Phase	HC_e (ppbC)	HC_d (ppbC)	FID THC_e (ppmC)	CH_{4e} (ppmC)	CO_{2e} (%)	CO_{em} (ppm)	R_a (%)	VMIX (ft^3)	$D_{phase\ n}$ (mile)
1	500	25	98	6	1.20	280	28	2846	3.584
2	100	25	22	4	0.95	87	25	4854	3.842
3	120	25	29	5	1.07	101	24	2840	3.586

For Phase 1:

   DF   = $13.47 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}]$
                 (see section 36, DF Calc.)

   $NMHC_e$ =   FID $THC_e - (r_{CH_4} * CH_{4e})$
          =   98 ppmC - (1.04 * 6 ppmC)
          =   92 ppmC

   CO   = $(1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$
   NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.
          =   (1 - (0.01925) * 1.2% - 0.000323 * 28%) * 280 ppm
          =   271 ppm

   DF   = $13.47 / [1.2\% + (92\ ppmC + 6\ ppmC + 271\ ppm) * 10^{-4}]$
          =   10.89

HC_{conc} = HC_e - (HC_d * (1 - (1 / DF)))

= 500 ppbC - (25 ppbC * (1 - (1 / 10.89)))

= 477 ppbC

Mol. Wt. of C_6H_6 = (6 * 12.01115) + (6 * 1.00797)

= 78.11472 g/mole

HC_{dens} = (Mol. Wt. * conversion of liter to ft^3) / (Mol. Vol.)

= (78.11472 g/mole * 28.316 liter/ft^3) / 24.055 liter/mole

= 91.952 g/ft^3

$HC_{mass\ n}$ = (HC_{conc} * HC_{dens} * VMIX * 10^{-6}) / (Carbon No.)

$HC_{mass\ 1}$ = (477 ppbC * 91.952 g/ft^3 * 2846 ft^3 * 10^{-6}) / 6

= 20.8 mg

Similarly, for Phase 2: Hc_{mass} = 5.7 mg

and for Phase 3: Hc_{mass} = 4.2 mg

Therefore,

$$HC_{wm} = 0.43 * \left(\frac{HC_{mass1} + HC_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{HC_{mass3} + HC_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$HC_{wm} = 0.43 * \left(\frac{20.8\,mg + 5.7\,mg}{3.584\,miles + 3.842\,miles} \right) + 0.57 * \left(\frac{4.2\,mg + 5.7\,mg}{3.586\,miles + 3.842\,miles} \right)$$

HC_{wm} = 2.3 mg/mile (benzene weighted mass emissions)

45. ALCOHOL MASS EMISSIONS CALCULATION

45.1. INTRODUCTION

Vehicular emissions are measured according to the (FTP [Ref. 1]. For each of the three phases of the FTP, a set of two impingers is used to collect alcohol emissions in the dilute exhaust. A fourth set of two impingers is used to collect a composite dilution air (background) alcohol sample from all three phases of the FTP. All impingers are analyzed according to Method No. 1001 to determine the alcohol concentration in each impinger. The measured alcohol concentrations are used in the following equations to calculate the weighted mass emissions of alcohol compounds.

45.2. ALCOHOL MASS EMISSIONS CALCULATION PER TEST PHASE

45.2.1 $ROH_{mass\ n}$ = $(ROH_{conc} * ROH_{dens} * VMIX * 10^{-6})$ / (Carbon No.)

45.2.2 ROH_{conc} = $ROH_e - (ROH_d * (1 - (1 / DF)))$
NOTE: If ROH_{conc} is calculated to be less than zero, then $ROH_{conc} = 0$.

45.2.3 ROH_e = $(Imass_e / Ivol_e) * (Mol.\ Vol.\ /\ Mol.\ Wt.)$

45.2.4 $Imass_e$ = $(Iconc_{e1} + Iconc_{e2})$ * Dens$_{ROH}$ * $Ivol_r$

45.2.5 $Ivol_e$ = $Ivol_{em} * (293.16^oK / Itemp_e) * (P_B / 760\ mm\ Hg)$

45.2.6 ROH_d = $(Imass_d / Ivol_d) * (Mol.\ Vol.\ /\ Mol.\ Wt.)$

45.2.7 $Imass_d$ = $(Iconc_{d1} + Iconc_{d2})$ * Dens$_{ROH}$ * $Ivol_r$

45.2.8 $Ivol_d$ = $Ivol_{dm} * (293.16^oK / Itemp_d) * (P_B / 760\ mm\ Hg)$

45.3. WEIGHTED ALCOHOL MASS EMISSIONS CALCULATION

$$ROH_{wm} = 0.43 * \left(\frac{ROH_{mass1} + ROH_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{ROH_{mass3} + ROH_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

45.4 SAMPLE CALCULATION

45.4.1 Alcohol emissions from an ~~M85~~ E85 fueled vehicle are collected in three sets of dilute exhaust impingers and one set of dilution air impingers during the FTP. Gas chromatography is used to determine the ~~methanol~~ alcohol concentration in each impinger. This is the same vehicle test as the example in section 3.3. Calculate the weighted ~~methanol~~ mass emissions based on the following data, along with the data presented in section 3.3:

Test Phase	$Ivol_r$ (mL)	$Iconc_{e1}$ (µg/mL)	$Iconc_{e2}$ (µg/mL)	$Ivol_{em}$ (liter)	$Iconc_{d1}$ (µg/mL)	$Iconc_{d2}$ (µg/mL)	$Ivol_{dm}$ (liter)	$Itemp_e$ (°K)	$Itemp_d$ (°K)
1	15	4.984 ~~2.24~~	0.106 ~~0.05~~	8.18 ~~3.90~~	0 ~~0.07~~	0 ~~0.01~~	31.16 ~~13.50~~	294.26 ~~295~~	294.26 ~~294~~
2	15	0 ~~0.29~~	0 ~~0.06~~	14.65 ~~6.50~~	0 ~~0.07~~	0 ~~0.01~~	31.16 ~~13.50~~	294.26 ~~297~~	294.26 ~~294~~
3	15	0 ~~0.32~~	0 ~~0.02~~	8.67 ~~4.00~~	0 ~~0.07~~	0 ~~0.01~~	31.16 ~~13.50~~	294.26 ~~298~~	294.26 ~~294~~

Test Phase	$D_{phase\ n}$ (mile)	DF	P_B (mm HG)	VMIX (ft3)
1	3.591	14.27	760	3495
2	3.846	22.15	760	5799
3	3.591	17.33	760	3484

~~Test Phase~~	~~FID THC$_e$ (ppmC)~~	~~CH$_{4e}$ (ppmC)~~	~~CO$_{2e}$ (%)~~	~~CO$_{em}$ (ppm)~~	~~R$_a$ (%)~~	~~VMIX (ft^3)~~	~~D$_{phase\ n}$ (mile)~~	~~P$_B$ (mmHg)~~	~~HCHO$_e$ (ppm)~~
~~1~~	~~82~~	~~9~~	~~1.5~~	~~250~~	~~30~~	~~2834~~	~~3.581~~	~~760~~	~~0.81~~
~~2~~	~~19~~	~~5~~	~~0.7~~	~~20~~	~~32~~	~~4862~~	~~3.845~~	~~760~~	~~0.09~~
~~3~~	~~22~~	~~6~~	~~0.8~~	~~32~~	~~29~~	~~2835~~	~~3.583~~	~~760~~	~~0.10~~

Ethanol

For Phase 1:

$$Imass_e = (Iconc_{e1} + Iconc_{e2}) \text{ ~~* Dens$_{ROH}$~~} * Ivol_r$$
$$= (4.984\ \mu g/mL + 0.106\ \mu g/mL) * 15\ mL$$
$$= 76.35\ \mu g$$

$$= \text{~~(2.24 µg/mL + 0.05 µg/mL) * 0.7914 g/mL *~~}$$
$$\text{~~15 mL * 10^6 µg/g~~}$$
$$= \text{~~27.2 µg~~}$$

Mol. Wt. of C_2H_5OH = $(2 * 12.01115) + (6 * 1.00797) + (1 * 15.9994)$
$$= 46.06952\ g/mole$$

~~Mol. Wt. of CH$_3$OH = (1 * 12.01115) + (4 * 1.00797) + (1 * 15.9994)~~
~~= 32.0428 g/mole~~

$$Ivol_e = Ivol_{em} * (293/16°\ K\ /\ Itemp_e) * (P_B / 760\ mm\ Hg)$$
$$= 8.18\ liter * (293.16°K / 294.26°\ K) * (760\ mm\ Hg / 760\ mm\ Hg)$$
$$= 8.15\ liters$$

$$= \text{~~3.90 liter * (293.16°K / 295° K) * (760 mm Hg / 760 mm Hg)~~}$$
$$= \text{~~3.88 liter~~}$$

$$ROH_e = (Imass_e / Ivol_e) * (Mol.\ Vol.\ /\ Mol.\ Wt.)$$

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$= \quad$ (76.35 µg / 8.15 liter) * (24.055 liter/mole / 46.06952 g/mole)

$= \quad$ 4.89 ppm

~~$= \quad$ (27.2*10^{-6} g / 3.88 liter) * (24.055 liter/mole / 46.06952 g/mole)~~

~~$= \quad$ 5.27 ppmC~~

$Imass_d = \quad (Iconc_{d1} + Iconc_{d2})$ ~~* Dens$_{ROH}$~~ $* Ivol_r$

$= \quad$ (0 µg/mL + 0µg/mL) * 15 mL

$= \quad$ 0 µg

~~$= \quad$ (0.07 µg/mL + 0.01 µg/mL) * 0.7914 g/ml * 15 ml * 10^6 µg/g~~

~~$= \quad$ 0.95 µg~~

$Ivol_d = \quad Ivol_{dm} * (293.16^o$ K $/ Itemp_d) * (P_B / 760$ mm Hg$)$

$= \quad$ 31.16 liter * (293.16^{o}K / 294.26^{o}K) * (760 mm Hg / 760 mm Hg)

$= \quad$ 31.04 liters

~~$= \quad$ 13.50 liter * (293.16^{o}K / 294°K) * (760 mm Hg / 760 mm Hg)~~

~~$= \quad$ 13.46 liter~~

$ROH_d = \quad (Imass_d / Ivol_d) * ($Mol. Vol. / Mol. Wt.$)$

$= \quad$ (0 µg / 31.46 liter) * (24.055 liter/mole / 46.06952 g/mole)

$= \quad$ 0 ppm

~~$= \quad$ (0.95*10^{-6} g/ 13.46 liter) * (24.055 liter/mole / 32.0428 g/mole)~~

~~$= \quad$ 0.05 ppmC~~

$\underline{DF \quad = \quad 14.2688}$ (as calculated in section 3.3)

~~$$DF = \frac{12.02}{CO_{2e} + \left(NMHC_e + CH_{4e} + CO_e + ROH_e + HCHO_e\right)*10^{-4}}$$~~

~~(see section 6, DF Calc.)~~

~~$NMHC_e \quad = \quad$ FID THC$_e$ - (r_{CH_4} * CH$_{4e}$) - (r_{CH_3OH} * ROH$_e$)~~

~~$= \quad$ 82 ppmC - (1.04 * 9 ppmC) - (0.66 * 5.27 ppmC)~~

~~$= \quad$ 69 ppmC~~

~~$CO_e \quad = \quad$ (1 - (0.01 + 0.005 * HCR) * CO$_{2e}$ - 0.000323 * R$_a$) * CO$_{em}$~~
~~NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO$_{em}$ must be substituted directly for CO$_e$.~~

~~$= \quad$ (1 - (0.02705) * 1.5% - 0.000323 * 30%) * 250 ppm~~

~~$= \quad$ 237 ppm~~

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$$\cancel{DF} = \frac{12.02}{1.5\% + (69\,\text{ppmC} + 9\,\text{ppmC} + 237\,\text{ppmC} + 5.27\,\text{ppmC} + 0.81\,\text{ppm}) * 10^{-4}}$$

$$
\begin{aligned}
ROH_{conc} &= ROH_e - (ROH_d * (1 - (1 / DF))) \\
&= \underline{4.89\,\text{ppm} - (0\,\text{ppmC} * (1 - (1 / 14.27)))} \\
&= \underline{4.89\,\text{ppm}}
\end{aligned}
$$

$$
\begin{aligned}
&= \quad \cancel{5.27\,\text{ppmC} - (0.05\,\text{ppmC} * (1 - (1 / 7.84)))} \\
&= \quad \cancel{5.23\,\text{ppmC}}
\end{aligned}
$$

$$
\begin{aligned}
ROH_{dens} &= (\text{Mol. Wt.} * \text{conversion of liter to ft}^3) / (\text{Mol. Vol.}) \\
&= \underline{(46.06952\,\text{g/mole} * 28.316\,\text{liter/ft}^3) / 24.055\,\text{liter/mole}} \\
&= \underline{54.23007808\,\text{g/ft}^3}
\end{aligned}
$$

$$
\begin{aligned}
&= \quad \cancel{(32.0428\,\text{g/mole} * 28.316\,\text{liter/ft}) / 24.055\,\text{liter/mole}} \\
&= \quad \cancel{37.719\,\text{g/ft}^3}
\end{aligned}
$$

$$\underline{VMIX = 3495\,\text{ft}^3 \ \text{(from section 3.3)}}$$

$$
\begin{aligned}
ROH_{mass\,n} &= (ROH_{conc} * ROH_{dens} * VMIX * 10^{-6}) \cancel{/ (\text{Carbon No.})} \\
ROH_{mass\,1} &= \underline{(4.89\,\text{ppmC} * 54.23\,\text{g/ft}^3 * 3495\,\text{ft}^3 * 10^{-6})} \\
&= \underline{0.93\,\text{g}}
\end{aligned}
$$

$$
\begin{aligned}
&= \quad \cancel{(5.23\,\text{ppmC} * 37.719\,\text{g/ft}^3 * 2834\,\text{ft}^3 * 10^{-6}) / 1} \\
&= \quad \cancel{0.56\,\text{g}}
\end{aligned}
$$

Similarly, for Phase 2: $ROH_{mass\,2} = \underline{0}\ \cancel{0.08}\ \text{g}$
and for Phase 3: $ROH_{mass\,3} = \underline{0}\ \cancel{0.08}\ \text{g}$

Therefore,

$$ROH_{wm} = 0.43 * \left(\frac{ROH_{mass1} + ROH_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{ROH_{mass3} + ROH_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$ROH_{wm} = 0.43 * \left(\frac{0.93\,\text{g} + 0\,\text{g}}{3.591\,\text{miles} + 3.846\,\text{miles}} \right) + 0.57 * \left(\frac{0\,\text{g} + 0\,\text{g}}{3.591\,\text{miles} + 3.846\,\text{miles}} \right)$$

$$\cancel{ROH_{wm} = 0.43 * \left(\frac{0.56\,\text{mg} + 0.08\,\text{mg}}{3.581\,\text{miles} + 3.845\,\text{miles}} \right) + 0.57 * \left(\frac{0.08\,\text{mg} + 0.08\,\text{mg}}{3.583\,\text{miles} + 3.845\,\text{miles}} \right)}$$

$$\underline{ROH_{wm} = 0.045\,\text{g/mile} \ \text{(ethanol weighted mass emissions)}}$$

$$\cancel{ROH_{wm} = 0.05\,\text{g} \ \text{(methanol weighted mass emissions)}}$$

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56. CARBONYL MASS EMISSIONS CALCULATIONS

56.1. INTRODUCTION

Vehicular emissions are measured according to the FTP [Ref. 1]. For each of the three phases of the FTP, a set of two impingers (or cartridges) is used to collect carbonyl emissions in the dilute exhaust. A fourth set of two impingers (or cartridges) is used to collect a composite dilution air (background) carbonyl sample from all three phases of the FTP. All impingers (or cartridges) are analyzed according to Method No. 1004 to determine the mass of individual carbonyl compounds in each impinger (or cartridge). The measured carbonyl masses are used in the following equations to calculate the weighted mass emissions of each carbonyl compound.

56.2. CARBONYL MASS EMISSIONS CALCULATION PER TEST PHASE

56.2.1 $RHO_{mass\ n} = (RHO_{conc} * RHO_{dens} * VMIX * 10^{-6})$

56.2.2 $RHO_{conc} = RHO_e - (RHO_d * (1 - (1 / DF)))$
NOTE: If RHO_{conc} is calculated to be less than zero, then $RHO_{conc} = 0$.

56.2.3 $RHO_e = (Imass_e / Ivol_e) * (Mol.\ Vol. / Mol.\ Wt.)$

56.2.4 $Imass_e = Iconc_{ce} * Ivol_c$

56.2.~~4~~5 $Ivol_e = Ivol_{em} * (293.16^{o}K / Itemp_e) * (P_B / 760\ mm\ Hg)$

56.2.~~5~~6 $RHO_d = (Imass_d / Ivol_d) * (Mol.\ Vol. / Mol.\ Wt.)$

56.2.7 $Imass_d = Iconc_{cd} * Ivol_c$

56.2.~~6~~8 $Ivol_d = Ivol_{dm} * (293.16^{o}K / Itemp_d) * (P_B / 760\ mm\ Hg)$

56.3. WEIGHTED CARBONYL MASS EMISSIONS CALCULATION

$$RHO_{wm} = 0.43 * \left(\frac{RHO_{mass1} + RHO_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{RHO_{mass3} + RHO_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

56.4. SAMPLE CALCULATION

56.4.1 Carbonyl emissions from ~~a CNG~~ an E85 vehicle are collected in three sets of dilute exhaust impingers and one set of dilution air impingers during the FTP. HPLC is used to determine the ~~formaldehyde~~ carbonyl mass in each impinger. This is the same vehicle test as the example in section 3.3. Calculate the weighted formaldehyde and

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acetaldehyde mass emissions based on the following data, along with the data presented in section 3.3:

Test Phase	$Ivol_c$ (ml)	Formaldehyde		$Ivol_{em}$ (liter)	Acetaldehyde		$Ivol_{dm}$ (liter)	$Itemp_e$ (°K)	$Itemp_d$ (°K)
		$Iconc_{ce}$ (µg/mL)	$Iconc_{cd}$ (µg/mL)		$Iconc_{ce}$ (µg/mL)	$Iconc_{cd}$ (µg/mL)			
1	4.4	0.387	0.006	8.47	4.114	0.006	8.23	294.26	294.26
2	4.4	0.048	0.016	15.35	0.013	0.009	13.88	294.26	294.26
3	4.4	0.016	0.006	9.01	0.012	0.005	8.16	294.26	294.26

~~Test Phase~~	~~$Ivol_r$ (mL)~~	~~$Imass_e$ (µg)~~	~~$Ivol_{em}$ (liter)~~	~~$Imass_d$ (µg)~~	~~$Ivol_{dm}$ (liter)~~	~~$Itemp_e$ (°K)~~	~~$Itemp_d$ (°K)~~
~~1~~	~~15~~	~~2.45~~	~~8.49~~	~~0.17~~	~~31.57~~	~~295~~	~~292~~
~~2~~	~~15~~	~~0.76~~	~~14.55~~	~~0.17~~	~~31.57~~	~~298~~	~~292~~
~~3~~	~~15~~	~~0.64~~	~~4.00~~	~~0.17~~	~~31.57~~	~~298~~	~~292~~

Test Phase	$D_{phase\ n}$ (mile)	DF	P_B (mm HG)	VMIX (ft3)
1	3.591	14.27	760	3495
2	3.846	22.15	760	5799
3	3.591	17.33	760	3484

~~Test Phase~~	~~FID THC_e (ppmC)~~	~~CH_{4e} (ppmC)~~	~~CO_{2e} (%)~~	~~CO_{em} (ppm)~~	~~R_a (%)~~	~~VMIX (ft³)~~	~~$D_{phase\ n}$ (mile)~~	~~P_B (mmHg)~~
~~1~~	~~132~~	~~108~~	~~0.9~~	~~8~~	~~68~~	~~2866~~	~~3.581~~	~~760~~
~~2~~	~~4~~	~~3~~	~~0.1~~	~~4~~	~~67~~	~~4841~~	~~3.845~~	~~760~~
~~3~~	~~22~~	~~9~~	~~0.5~~	~~5~~	~~65~~	~~2837~~	~~3.583~~	~~760~~

Formaldehyde

For Phase 1:

$$Imass_e = Iconc_{ce} * Ivol_c$$
$$= 0.387\ µg/mL * 4.4\ mL$$
$$= 1.70\ µg$$

Mol. Wt. of HCHO = (1 * 12.01115) + (2 * 1.00797) + (1 * 15.9994)
$$= 30.0268\ g/mole$$

$$Ivol_e = Ivol_{em} * (293/16°\ K\ /\ Itemp_e) * (P_B\ /\ 760\ mm\ Hg)$$
$$= 8.47\ liter * (293.16°K\ /\ 294.26°K) * (760\ mm\ Hg\ /\ 760\ mm\ Hg)$$
$$= 8.44\ liter$$

$$\text{~~}= 8.49\ liter * (293.16°K\ /\ 295°K) * (760\ mm\ Hg\ /\ 760\ mm\ Hg)\text{~~}$$
$$\text{~~}= 8.44\ liter\text{~~}$$

$$RHO_e = (Imass_e / Ivol_e) * (Mol. Vol. / Mol. Wt.)$$
$$= (1.70 \, \mu g / 8.44 \, liter) * (24.055 \, liter/mole / 30.0268 \, g/mole)$$
$$= 0.16 \, ppm$$

~~$= (2.45*10^{-6} g / 8.44 \, liter) * (24.055 \, liter/mole / 30.0268 \, g/mole)$~~
~~$= 233 \, ppb$~~

$$Imass_d = Iconc_{cd} * Ivol_c$$
$$= 0.006 \, \mu g/mL * 4.4 \, mL$$
$$= 0.026 \, \mu g$$

$$Ivol_d = Ivol_{dm} * (293.16^o K / Itemp_d) * (P_B / 760 \, mm \, Hg)$$
$$= 8.23 \, liter * (293.16^o K / 294.26^o K) * (760 \, mm \, Hg / 760 \, mm \, Hg)$$
$$= 8.20 \, liter$$

~~$= 31.57 \, liter * (293.16^o K / 292^o K) * (760 \, mm \, Hg / 760 \, mm \, Hg)$~~
~~$= 31.70 \, liter$~~

$$RHO_d = (Imass_d / Ivol_d) * (Mol. Vol. / Mol. Wt.)$$
$$= (0.026 \, \mu g / 8.20 \, liter) * (24.055 \, liter/mole / 30.0268 \, g/mole)$$
$$= 0.00258 \, ppm$$

~~$= (0.17*10^{-6} g / 31.70 \, liter)*(24.055 \, liter/mole / 30.0268 \, g/mole)$~~
~~$= 4 \, ppb$~~

$$DF = 14.2688$$

~~$DF = 9.77 / [CO_{2e} + (NMHC_e + CH_{4e} + CO^e) * 10^{-4}]$~~
~~(see section 6, DF Calc.)~~

~~$NMHC_e = FID \, THC_e - (r_{CH_4} * CH_{4e})$~~
~~$= 132 \, ppmC - (1.04 * 108 \, ppmC)$~~
~~$= 20 \, ppmC$~~

~~$CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$~~
~~NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.~~

~~$= (1 - 0.02890 * 0.9\% - 0.000323 * 68\%) * 8 \, ppm$~~
~~$= 7.6 \, ppm$~~

~~$DF = 9.77 / [0.9\% + (20 \, ppmC + 108 \, ppmC + 7.6 \, ppm) * 10^{-4}]$~~
~~$= 10.69$~~

$$RHO_{conc} = RHO_e - (RHO_d * (1 - (1 / DF)))$$

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$$= \quad 0.162 \text{ ppm} - (0.00258 \text{ ppm} * (1 - (1 / 14.27)))$$
$$= \quad 0.1596 \text{ ppm}$$

$$= \quad \cancel{233 \text{ ppb} - (4 \text{ ppb} * (1 - (1 / 10.69)))}$$
$$= \quad \cancel{229 \text{ ppb}}$$

$$RHO_{dens} \quad = \quad (\text{Mol. Wt.} * \text{conversion of liter to ft}^3) / (\text{Mol. Vol.})$$
$$= \quad (30.0268 \text{ g/mole} * 28.316 \text{ liter/ft}^3) / 24.055 \text{ liter/mole}$$
$$= \quad 35.35 \text{ g/ft}^3$$

$$\underline{VMIX \quad = \quad 3495 \text{ ft}^3}$$

$$RHO_{mass\,n} \quad = \quad (RHO_{conc} * RHO_{dens} * VMIX * 10^{-6})$$
$$RHO_{mass\,1} \quad = \quad (0.1596 \text{ ppm} * 35.35 \text{ g/ft}^3 * 3495 \text{ ft}^3 * 10^{-6} * 1000 \text{ mg/g})$$
$$= \quad 19.718 \text{ mg}$$

$$= \quad \cancel{(229 \text{ ppb} * 35.35 \text{ g/ft}^3 * 2866 \text{ ft}^3 * 10^{-6})}$$
$$= \quad \cancel{23.2 \text{ mg}}$$

Similarly, for Phase 2: $\qquad RHO_{mass\,2} = \qquad \underline{1.457}$ ~~6.6~~ mg
and for Phase 3: $\qquad RHO_{mass\,3} = \qquad \underline{0.472}$ ~~12.7~~ mg

Therefore,

$$RHO_{wm} = 0.43 * \left(\frac{RHO_{mass1} + RHO_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{RHO_{mass3} + RHO_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$RHO_{wm} = 0.43 * \left(\frac{19.718 \text{ mg} + 1.457 \text{ mg}}{3.591 \text{ miles} + 3.846 \text{ miles}} \right) + 0.57 * \left(\frac{0.472 \text{ mg} + 1.457 \text{ mg}}{3.591 \text{ miles} + 3.846 \text{ miles}} \right)$$

$$\cancel{RHO_{wm} = 0.43 * \left(\frac{23.2 \text{ mg} + 6.6 \text{ mg}}{3.581 \text{ miles} + 3.845 \text{ miles}} \right) + 0.57 * \left(\frac{12.7 \text{ mg} + 6.6 \text{ mg}}{3.583 \text{ miles} + 3.845 \text{ miles}} \right)}$$

$$RHO_{wm} = \underline{1.371}\ \cancel{3.2} \text{ mg/mi} \quad \text{(formaldehyde weighted mass emissions)}$$

Acetaldehyde

Similarly,

Phase 1: $\qquad RHO_{mass\,1} = 212 \text{ mg}$
Phase 2: $\qquad RHO_{mass\,2} = 0.165 \text{ mg}$
Phase 3: $\qquad RHO_{mass\,3} = 0.329 \text{ mg}$

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$$RHO_{wm} = 0.43 * \left(\frac{212 \, mg + 0.165 \, mg}{3.591 \, miles + 3.846 \, miles} \right) + 0.57 * \left(\frac{0.329 \, mg + 0.165 \, mg}{3.591 \, miles + 3.846 \, miles} \right)$$

RHO_{wm} = 0.0123 mg/mi (acetaldehyde weighted mass emissions)

5.4.2 ~~Carbonyl emissions from a gasoline vehicle are collected in three sets of dilute exhaust cartridges and dilution air cartridges during the FTP. HPLC is used to determine the formaldehyde mass in each cartridge. Calculate the weighted formaldehyde mass emissions based on the following data:~~

~~Test Phase~~	~~$Iconc_{ee}$ (µg/mL)~~	~~$Iconc_{ed}$ (µg/mL)~~	~~$Iconc_{blk}$ (µg/mL)~~	~~$Ivol_{dm}$ (liter)~~	~~$Ivol_{em}$ (liter)~~	~~$Itemp_e$ (°K)~~	~~$Itemp_d$ (°K)~~
~~1~~	~~1.212~~	~~0.028~~	~~0.0~~	~~8.61~~	~~8.57~~	~~294.26~~	~~294.26~~
~~2~~	~~0.334~~	~~0.043~~	~~0.0~~	~~14.91~~	~~13.83~~	~~294.26~~	~~294.26~~
~~3~~	~~0.172~~	~~0.026~~	~~0.0~~	~~8.68~~	~~8.74~~	~~294.26~~	~~294.26~~

~~Test Phase~~	~~FID THC_e (ppmC)~~	~~CH_{4e} (ppmC)~~	~~CO_{2e} (%)~~	~~CO_{em} (ppm)~~	~~R_a (%)~~	~~VMIX (ft^3)~~	~~$D_{phase\,n}$ (mile)~~	~~P_B (mmHg)~~
~~1~~	~~132~~	~~108~~	~~0.9~~	~~8~~	~~68~~	~~2866~~	~~3.581~~	~~760~~
~~2~~	~~4~~	~~3~~	~~0.1~~	~~4~~	~~67~~	~~4841~~	~~3.845~~	~~760~~
~~3~~	~~22~~	~~9~~	~~0.5~~	~~5~~	~~65~~	~~2837~~	~~3.583~~	~~760~~

~~For all three phases $Ivol_c$ = 4.4 mL~~

~~For Phase 1:~~

~~$Imass_d = (Iconc_{ed} - Iconc_{blk}) * Ivol_c$~~

~~$Imass_d = (0.028 - 0.0)$ µg/mL * 4.4 mL = 0.1232 µg~~

~~$Imass_e = (Iconc_{ee} - Iconc_{blk}) * Ivol_c$~~

~~$Imass_e = (1.212 - 0.0)$ µg/mL * 4.4 mL = 5.33 µg~~

~~Mol. Wt. of HCHO = (1 * 12.01115) + (2 * 1.00797) + (1 * 15.9994)~~
~~= 30.0265 g/mole~~

~~$Ivol_e = Ivol_{em} * (293/16° \, K / Itemp_e) * (P_B / 760 \, mm \, Hg)$~~

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$$\text{= 8.57 liter * (293.16}^\circ\text{K / 294.26}^\circ\text{K) * (760 mm Hg / 760 mm Hg)}$$
$$\text{= 8.54 liter}$$

$$RHO_e = (Imass_e / Ivol_e) * (\text{Mol. Vol. / Mol. Wt.})$$
$$= (5.33*10^{-6} \text{ g} / 8.54 \text{ liter}) * (24.055 \text{ liter/mole} / 30.0265 \text{ g/mole})$$
$$= 500 \text{ ppb}$$

$$Ivol_d = Ivol_{dm} * (293.16^\circ K / Itemp_d) * (P_B / 760 \text{ mm Hg})$$
$$= 8.61 \text{ liter} * (293.16^\circ K / 294.26^\circ K) * (760 \text{ mm Hg} / 760 \text{ mm Hg})$$
$$= 8.58 \text{ liter}$$

$$RHO_d = (Imass_d / Ivol_d) * (\text{Mol. Vol. / Mol. Wt.})$$
$$= (0.1232*10^{-6} \text{ g} / 8.58 \text{ liter})*(24.055 \text{ liter/mole} / 30.0265 \text{ g/mole})$$
$$= 11.5 \text{ ppb}$$

$$DF = 9.77 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}]$$
(see section 6, DF Calc.)

$$NMHC_e = \text{FID THC}_e - (r_{CH_4} * CH_{4e})$$
$$= 132 \text{ ppmC} - (1.04 * 108 \text{ ppmC})$$
$$= 20 \text{ ppmC}$$

$$CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$$
NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.

$$= (1 - 0.02890 * 0.9\% - 0.000323 * 68\%) * 8 \text{ ppm}$$
$$= 7.6 \text{ ppm}$$

$$DF = 9.77 / [0.9\% + (20 \text{ ppmC} + 108 \text{ ppmC} + 7.6 \text{ ppm}) * 10^{-4}]$$
$$= 10.69$$

$$RHO_{conc} = RHO_e - (RHO_d * (1 - (1 / DF)))$$
$$= 500 \text{ ppb} - (11.5 \text{ ppb} * (1 - (1 / 10.69)))$$
$$= 489.6 \text{ ppb (formaldehyde)}$$

$$RHO_{dens} = (\text{Mol. Wt. * conversion of liter to ft}^3) / (\text{Mol. Vol.})$$
$$= (30.0265 \text{ g/mole} * 28.316 \text{ liter/ft}^3) / 24.055 \text{ liter/mole}$$
$$= 35.35 \text{ g/ft}^3$$

$$RHO_{mass \, n} = (RHO_{conc} * RHO_{dens} * VMIX * 10^{-6})$$

$$RHO_{mass \, 1} = (489.6 \text{ ppb} * 35.35 \text{ g/ft}^3 * 2866 \text{ ft}^3 * 10^{-6})$$
$$= 49.6 \text{ mg (formaldehyde)}$$

Similarly, for Phase 2: $RHO_{mass \, 2} = 12.9 \text{ mg}$

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and similarly for Phase 3: $RHO_{mass\,3} = 5.6$ mg

Therefore,

$$RHO_{wm} = 0.43 * \left(\frac{RHO_{mass1} + RHO_{mass2}}{D_{phase1} + D_{phase2}}\right) + 0.57 * \left(\frac{RHO_{mass3} + RHO_{mass2}}{D_{phase3} + D_{phase2}}\right)$$

$$RHO_{wm} = 0.43 * \left(\frac{49.6 \text{ mg} + 12.9 \text{ mg}}{3.581 \text{ miles} + 3.845 \text{ miles}}\right) + 0.57 * \left(\frac{5.6 \text{ mg} + 12.9 \text{ mg}}{3.583 \text{ miles} + 3.845 \text{ miles}}\right)$$

$RHO_{wm} = 5.04$ mg/mi (formaldehyde weighted mass emissions)

6.   DILUTION FACTOR CALCULATION

6.1.   For Non-Alcohol Fueled Vehicles

6.1.1 $$DF = \frac{100 * \left(\dfrac{x}{x + y/2 + 3.76*(x + y/4 - z/2)}\right)}{CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}}$$

(where fuel composition is $C_xH_yO_z$, as measured for the fuel used.)

6.1.2 $CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$
NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.

a)   For gasoline, $CH_{1.85}$, where x = 1, y = 1.85, and z = 0:
$DF = 13.47 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}$
$CO_e = (1 - 0.01925 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

b)   For Phase 2 gasoline, $CH_{1.94}$, where x = 1, y = 1.94 and z = 0.017,
$DF = 13.29 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}$
$CO_e = (1 - 0.01970 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

c)   For LPG, $CH_{2.64}$, where x = 1, y = 2.64, z = 0:
$DF = 11.68 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}$
$CO_e = (1 - 0.02320 * CO_{2e} - 0.000323 * R_a) * CO_{em}$

d)   For CNG, $CH_{3.78}$, where x = 1, y = 3.78, and z = 0.016:

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$$\sim\sim DF = 9.83 \ / \ [[CO_{2e} + (NMHC_e + CH_{4e} + CO_e) * 10^{-4}]$$
$$CO_e = (1 - 0.02890 * CO_{2e} - 0.000323 * R_a) * CO_{em} \sim\sim$$

~~6.2.~~ **~~For Alcohol Fueled Vehicles~~**~~:~~

~~6.2.1~~ $$DF = \dfrac{100 * \left(\dfrac{x}{x + y/2 + 3.76*(x + y/4 - z/2)}\right)}{CO_{2e} + (NMHC_e + CH_{4e} + CO_e + ROH_e + HCHO_e)*10^{-4}}$$

~~(where fuel composition is $C_xH_yO_z$, as measured for the fuel used.)~~

~~6.2.2~~ ~~$CO_e = (1 - (0.01 + 0.005 * HCR) * CO_{2e} - 0.000323 * R_a) * CO_{em}$~~
~~NOTE: If a CO instrument which meets the criteria specified in CFR 40, 86.111 is used and the conditioning column has been deleted, CO_{em} must be substituted directly for CO_e.~~

~~a)~~ ~~For M100 (100% methanol), CH_3OH, where x = 1, y = 4, and z = 1:~~
~~$DF = 11.57 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + ROH_e + HCHO_e) * 10^{-4}]$~~
~~$CO_e = (1 - 0.03000 * CO_{2e} - 0.000323 * R_a) * CO_{em}$~~

~~b)~~ ~~For M85 (85% methanol, 15% indolene), $CH_{3.41}O_{0.72}$, where x = 1, y = 3.41, and z = 0.72:~~
~~$DF = 12.02 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + ROH_e + HCHO_e) * 10^{-4}]$~~
~~$CO_e = (1 - 0.02705 * CO_{2e} - 0.000323 * R_a) * CO_{em}$~~

~~c)~~ ~~For E100 (100% ethanol), C_2H_5OH, where x = 1, y = 3, and z = 0.5:~~
~~$DF = 12.29 / [CO_{2e} + (NMHC_e + CH_{4e} + CO_e + ROH_e + HCHO_e) * 10^{-4}]$~~
~~$CO_e = (1 - 0.02500 * CO_{2e} - 0.000323 * R_a) * CO_{em}$~~

7   NONMHC MASS EMISIONS CALCULATION

7.1   Non-oxygenated non-methane hydrocarbon is calculated from the FID NMHC measurement using the following equation:

$$NONMHC_{mass} = NMHC_{mass} - NMHC_{dens} * \sum\left(\frac{ROH_{mass}}{ROH_{dens}}\right)*r_{ROH} - NMHC_{dens} * \sum\left(\frac{RHO_{mass}}{RHO_{dens}}\right)*r_{RHO}$$

7.1.1   For the purpose of calculating NMOG for vehicles tested on exhaust emission test fuel containing ethanol:

7.1.1.1   The only alcohol included in the above calculation is ethanol.

7.1.1.2   The only carbonyl compounds included in the above calculation are formaldehyde and acetaldehyde.

7.2   FID Response Factors:

FID response factors are experimentally determined for each individual FID. The following values are used in the sample calculations and are presented for example only.

Oxygenated species	Response factor* (*RF*)
methanol	0.85
ethanol	0.756
formaldehyde	0
acetaldehyde	0.5

* Response factors are normalized to propane, i.e., propane has a response factor of 1.000.

7.3 Sample Calculation

Continuing from the same E85 test used in the alcohol and carbonyl calculations:

Test Phase	$NMHC_{mass\ n}$ (g)	$Ethanol_{mass\ n}$ (g)	$Formaldehyde_{mass\ n}$ (g)	$Acetaldehyde_{mass\ n}$ (g)
1	1.1220	0.09271	0.0197	0.212
2	0	0	0.001457	0.000165
3	0.0026	0	0.000472	0.000329

and

$$NMHC_{dens} = 17.44 \text{ g/ft}^3$$

$$NONMHC_{mass1} = NMHC_{mass1} - NMHC_{dens} * \sum \left(\frac{ROH_{mass1}}{ROH_{dens}} \right) * r_{ROH} - NMHC_{dens} * \sum \left(\frac{RHO_{mass1}}{RHO_{dens}} \right) * r_{RHO}$$

$$
\begin{aligned}
NONMHC_{mass1} &= 1.1220 - 17.44 \text{ g/ft}^3 * (0.9271 \text{ g} / 27.116 \text{ (g/ft}^3)) * 0.756 \\
&\quad - 17.44 \text{ g/ft}^3 * (0.0197 \text{ g} / 35.350 \text{ (g/ft}^3)) * 0 \\
&\quad - 17.44 \text{ g/ft}^3 * (0.212 \text{ g} / 25.929 \text{ (g/ft}^3)) * 0.5 \\
&= 1.1220 - 0.4508 - 0 - 0.0713 \\
&= 0.5999 \text{ g}
\end{aligned}
$$

$$
\begin{aligned}
NONMHC_{mass2} &= 0 - 17.44 \text{ g/ft}^3 * (0 \text{ g} / 27.116 \text{ (g/ft}^3)) * 0.756 \\
&\quad - 17.44 \text{ g/ft}^3 * (0.001457 \text{ g} / 35.350 \text{ (g/ft}^3)) * 0 \\
&\quad - 17.44 \text{ g/ft}^3 * (0.000165 \text{ g} / 25.929 \text{ (g/ft}^3)) * 0.5 \\
&= 0 - 0 - 0 - 0.000055 \\
&= 0 \text{ g}
\end{aligned}
$$

Note: Results that are less than zero are reported as zero.

$$\underline{NONMHC_{mass3}} = \underline{0.0026} - 17.44 \text{ g/ft}^3 * (0 \text{ g} / 27.116 \text{ (g/ft}^3)) * 0.756$$
$$\underline{- 17.44 \text{ g/ft}^3 * (0.000472 \text{ g} / 35.350 \text{ (g/ft}^3)) * 0}$$
$$\underline{- 17.44 \text{ g/ft}^3 * (0.000329 \text{ g} / 25.929 \text{ (g/ft}^3)) * 0.5}$$
$$= \underline{0.0026} - 0 - 0 - 0.000111$$
$$= \underline{0.00249 \text{ g}}$$

8   WEIGHTED HYDROCARBON MASS EMISSIONS CALCULATION

8.1   Weighted NMOG is determined using the following equation:

$$\underline{NMOG_{wm} = \sum NONMHC_{wm} + \sum ROH_{wm} + \sum RHO_{wm}}$$

where:

$$NONMHC_{wm} = 0.43 * \left(\frac{NONMHC_{mass1} + NONMHC_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{NONMHC_{mass3} + NONMHC_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$ROH_{wm} = 0.43 * \left(\frac{ROH_{mass1} + ROH_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{ROH_{mass3} + ROH_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

$$RHO_{wm} = 0.43 * \left(\frac{RHO_{mass1} + RHO_{mass2}}{D_{phase1} + D_{phase2}} \right) + 0.57 * \left(\frac{RHO_{mass3} + RHO_{mass2}}{D_{phase3} + D_{phase2}} \right)$$

     8.1.1   For the purpose of calculating NMOG for vehicles tested on exhaust emission test fuel containing ethanol:

     8.1.1.1   The only alcohol included in the weighted NMOG calculation is ethanol.

     8.1.1.2   The only carbonyl compounds included in the weighted NMOG calculation are formaldehyde and acetaldehyde.

8.2   Sample calculation

Continuing from the previous example:

Test Phase	$NONMHC_{mass\ n}$ (g)	$Ethanol_{mass\ n}$ (g)	$Formaldehyde_{mass\ n}$ (g)	$Acetaldehyde_{mass\ n}$ (g)	Distance (mile)
1	0.5999	0.9271	0.019718	0.212	3.591
2	0	0	0.001457	0.000165	3.846

| 3 | 0.00249 | 0 | 0.000472 | 0.000329 | 3.591 |

$$\text{NONMHC}_{wm} = 0.43 * \left(\frac{0.5999\,\text{g} + 0\,\text{g}}{3.591\,\text{miles} + 3.846\,\text{miles}} \right) + 0.57 * \left(\frac{0.00249\,\text{g} + 0\,\text{g}}{3.591\,\text{miles} + 3.846\,\text{miles}} \right)$$

NONMHC_{wm} = 0.03488 g/mile
Similarly, Ethanol_{wm} = 0.05360 g/mile
Similarly, Formaldehyde_{wm} = 0.00137 g/mile
Similarly, Acetaldehyde_{wm} = 0.01231 g/mile

With all the above information, the weighted mass emissions of non-methane organic gas can be calculated:

$$\text{NMOG}_{wm} = \sum \text{NONMHC}_{wm} + \sum \text{ROH}_{wm} + \sum \text{RHO}_{wm}$$

NMOG_{wm} = 0.03488 g/mile + 0.05360 g/mile + 0.00137 g/mile + 0.01231 g/mile
        = 0.102 g/mile

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APPENDIX 1

LIST OF COMPOUNDS

CAS #	COMPOUND	MIR

Alcohols

CAS #	COMPOUND	MIR
00067-56-1	methanol	~~0.71~~ 0.67
00064-17-5	ethanol	~~1.69~~ 1.53

Light End and Mid-Range Hydrocarbons
(Listed in approximate elution order)

CAS #	COMPOUND	MIR
00074-85-1	ethene	~~9.08~~ 9.00
00074-86-2	ethyne	~~1.25~~ 0.95
00074-84-0	ethane	~~0.31~~ 0.28
00115-07-1	propene	~~11.58~~ 11.66
00074-98-6	propane	~~0.56~~ 0.49
00463-49-0	1,2-propadiene	~~12.16~~ 8.45
00074-99-7	1-propyne	~~6.45~~ 6.72
00075-28-5	2-methylpropane	~~1.35~~ 1.23
00115-11-7	2-methylpropene	~~6.35~~ 6.29
00106-98-9	1-butene	~~10.29~~ 9.73
00106-99-0	1,3-butadiene	~~13.58~~ 12.61
00106-97-8	n-butane	~~1.33~~ 1.15
00624-64-6	trans-2-butene	~~13.91~~ 15.16
00463-82-1	2,2-dimethylpropane	~~1.68~~ 0.67
00107-00-6	1-butyne	~~6.20~~ 6.11
00590-18-1	cis-2-butene	~~13.22~~ 14.24
00563-45-1	3-methyl-1-butene	6.99
00078-78-4	2-methylbutane	~~1.68~~ 1.45
00503-17-3	2-butyne	~~16.33~~ 16.32
00109-67-1	1-pentene	~~7.79~~ 7.21
00563-46-2	2-methyl-1-butene	~~6.51~~ 6.40
00109-66-0	n-pentane	~~1.54~~ 1.31
00078-79-5	2-methyl-1,3-butadiene	~~10.69~~ 10.61
00646-04-8	trans-2-pentene	~~10.23~~ 10.56
00558-37-2	3,3-dimethyl-1-butene	~~6.06~~ 5.82
00627-20-3	cis-2-pentene	~~10.24~~ 10.38
00689-97-4	1-buten-3-yne	~~11.09~~ 10.48
00513-35-9	2-methyl-2-butene	~~14.45~~ 14.08
00542-92-7	1,3-cyclopentadiene	~~7.61~~ 6.98
00075-83-2	2,2-dimethylbutane	~~1.33~~ 1.17
00142-29-0	cyclopentene	~~7.38~~ 6.77
00691-37-2	4-methyl-1-pentene	~~6.26~~ 5.68

CAS #	COMPOUND	MIR
00760-20-3	3-methyl-1-pentene	~~6.22~~ 6.14
00287-92-3	cyclopentane	~~2.69~~ 2.39
00079-29-8	2,3-dimethylbutane	~~1.14~~ 0.97
01634-04-4	1-methyl-tert-butyl-ether	~~0.78~~ 0.73
00691-38-3	4-methyl-cis-2-pentene	~~8.44~~ 8.12
00107-83-5	2-methylpentane	~~1.80~~ 1.50
00674-76-0	4-methyl-trans-2-pentene	~~8.44~~ 8.12
00096-14-0	3-methylpentane	~~2.07~~ 1.80
00763-29-1	2-methyl-1-pentene	~~5.18~~ 5.26
00592-41-6	1-hexene	~~6.17~~ 5.49
00110-54-3	n-hexane	~~1.45~~ 1.24
13269-52-8	trans-3-hexene	~~8.16~~ 7.57
07642-09-3	cis-3-hexene	~~8.22~~ 7.61
04050-45-7	trans-2-hexene	~~8.44~~ 8.62
00616-12-6	3-methyl-trans-2-pentene	~~8.44~~ 13.17
00625-27-4	2-methyl-2-pentene	~~12.28~~ 11.00
01120-62-3	3-methylcyclopentene	~~8.65~~ 5.10
07688-21-3	cis-2-hexene	~~8.44~~ 8.31
00637-92-3	1-ethyl-tert-butyl-ether	~~2.11~~ 2.01
00922-62-3	3-methyl-cis-2-pentene	~~8.44~~ 12.49
00590-35-2	2,2-dimethylpentane	~~1.22~~ 1.12
00096-37-7	methylcyclopentane	~~2.42~~ 2.19
00108-08-7	2,4-dimethylpentane	~~1.65~~ 1.55
00464-06-2	2,2,3-trimethylbutane	~~1.32~~ 1.11
07385-78-6	3,4-dimethyl-1-pentene	~~4.56~~ 4.84
00693-89-0	1-methylcyclopentene	~~13.95~~ 12.49
00071-43-2	benzene	~~0.81~~ 0.72
03404-61-3	3-methyl-1-hexene	4.56 ~~4.41~~
00562-49-2	3,3-dimethylpentane	~~1.32~~ 1.20
00110-82-7	cyclohexane	~~1.46~~ 1.25
00591-76-4	2-methylhexane	~~1.37~~ 1.19
00565-59-3	2,3-dimethylpentane	~~1.55~~ 1.34
00110-83-8	cyclohexene	~~5.45~~ 5.00
00589-34-4	3-methylhexane	~~1.86~~ 1.61
01759-58-6	trans-1,3-dimethylcyclopentane	~~2.15~~ 1.94
02532-58-3	cis-1,3-dimethylcyclopentane	~~2.15~~ 1.94
00617-78-7	3-ethylpentane	~~1.63~~ 1.90
00822-50-4	trans-1,2-dimethylcyclopentane	1.99
00592-76-7	1-heptene	~~4.56~~ 4.43
00540-84-1	2,2,4-trimethylpentane	~~1.44~~ 1.26
14686-14-7	trans-3-heptene	~~6.96~~ 6.32
00142-82-5	n-heptane	~~1.28~~ 1.07
02738-19-4	2-methyl-2-hexene	~~6.96~~ 9.47
03899-36-3	3-methyl-trans-3-hexene	~~6.96~~ 9.72
14686-13-6	trans-2-heptene	~~7.33~~ 7.14

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CAS #	COMPOUND	MIR
00816-79-5	3-ethyl-2-pentene	~~6.96~~ 9.75
00107-39-1	2,4,4-trimethyl-1-pentene	~~3.45~~ 3.34
10574-37-5	2,3-dimethyl-2-pentene	~~6.96~~ 9.74
06443-92-1	cis-2-heptene	~~6.96~~ 7.16
00108-87-2	methylcyclohexane	~~1.99~~ 1.70
00590-73-8	2,2-dimethylhexane	~~1.13~~ 1.02
00107-40-4	2,4,4-trimethyl-2-pentene	~~5.85~~ 6.29
01640-89-7	ethylcyclopentane	~~2.27~~ 2.01
00592-13-2	2,5-dimethylhexane	~~1.68~~ 1.46
00589-43-5	2,4-dimethylhexane	~~1.80~~ 1.73
02815-58-9	1,2,4-trimethylcyclopentane	~~1.75~~ 1.53
00563-16-6	3,3-dimethylhexane	~~1.57~~ 1.24
00565-75-3	2,3,4-trimethylpentane	~~1.23~~ 1.03
00560-21-4	2,3,3-trimethylpentane	~~1.57~~ 1.02
00108-88-3	toluene	~~3.97~~ 4.00
00584-94-1	2,3-dimethylhexane	~~1.34~~ 1.19
00592-27-8	2-methylheptane	~~1.20~~ 1.07
00589-53-7	4-methylheptane	~~1.48~~ 1.25
00589-81-1	3-methylheptane	~~1.35~~ 1.24
15890-40-1	(1a,2a,3b)-1,2,3-trimethylcyclopentane	~~1.75~~ 1.63
00638-04-0	cis-1,3-dimethylcyclohexane	~~1.72~~ 1.52
02207-04-7	trans-1,4-dimethylcyclohexane	~~1.75~~ 1.47
03522-94-9	2,2,5-trimethylhexane	~~1.33~~ 1.13
02613-65-2	trans-1-methyl-3-ethylcyclopentane	~~1.75~~ 1.64
16747-50-5	cis-1-methyl-3-ethylcyclopentane	~~1.75~~ 1.64
00111-66-0	1-octene	~~3.45~~ 3.25
14850-23-8	trans-4-octene	~~5.90~~ 4.81
00111-65-9	n-octane	~~1.11~~ 0.90
13389-42-9	trans-2-octene	~~5.90~~ 6.00
02207-03-6	trans-1,3-dimethylcyclohexane	~~1.72~~ 1.52
07642-04-8	cis-2-octene	~~5.90~~ 4.81
01069-53-0	2,3,5-trimethylhexane	~~1.33~~ 1.22
02213-23-2	2,4-dimethylheptane	~~1.48~~ 1.38
02207-01-4	cis-1,2-dimethylcyclohexane	~~1.75~~ 1.41
01072-05-5	2,6-dimethylheptane	~~1.25~~ 1.04
01678-91-7	ethylcyclohexane	~~1.75~~ 1.47
00926-82-9	3,5-dimethylheptane	~~1.63~~ 1.56
00100-41-4	ethylbenzene	~~2.79~~ 3.04
03074-71-3	2,3-dimethylheptane	~~1.25~~ 1.09
00108-38-3	m-&p-xylene	~~8.49~~ 8.45
02216-34-4	4-methyloctane	~~1.08~~ 0.95
03221-61-2	2-methyloctane	~~0.96~~ 0.83
02216-33-3	3-methyloctane	~~1.25~~ 0.99
00100-42-5	styrene (ethenylbenzene)	~~1.95~~ 1.73
00095-47-6	o-xylene	~~7.49~~ 7.64

1-3

CAS #	COMPOUND	MIR
00124-11-8	1-nonene	~~2.76~~ 2.60
00111-84-2	n-nonane	~~0.95~~ 0.78
00098-82-8	(1-methylethyl)benzene	~~2.32~~ 2.52
15869-87-1	2,2-dimethyloctane	~~1.09~~ 0.83
04032-94-4	2,4-dimethyloctane	~~1.09~~ 1.03
02051-30-1	2,6-dimethyloctane	~~1.27~~ 1.08
00103-65-1	n-propylbenzene	~~2.20~~ 2.03
00620-14-4	1-methyl-3-ethylbenzene	~~6.61~~ 7.39
00622-96-8	1-methyl-4-ethylbenzene	~~6.61~~ 4.44
00108-67-8	1,3,5-trimethylbenzene	~~11.22~~ 11.76
00611-14-3	1-methyl-2-ethylbenzene	~~6.61~~ 5.59
00095-63-6	1,2,4-trimethylbenzene	~~7.18~~ 8.87
00124-18-5	n-decane	~~0.83~~ 0.68
00538-93-2	(2-methylpropyl)benzene	~~1.97~~ 2.36
00135-98-8	(1-methylpropyl)benzene	~~1.97~~ 2.36
00535-77-3	1-methyl-3-(1-methylethyl)benzene	~~5.92~~ 7.10
00526-73-8	1,2,3-trimethylbenzene	~~11.26~~ 11.97
00099-87-6	1-methyl-4-(1-methylethyl)benzene	~~5.92~~ 4.44
00496-11-7	2,3-dihydroindene (indan)	~~3.17~~ 3.32
00527-84-4	1-methyl-2-(1-methylethyl)benzene	~~5.92~~ 5.49
00141-93-5	1,3-diethylbenzene	~~5.92~~ 7.10
00105-05-5	1,4-diethylbenzene	~~5.92~~ 4.43
01074-43-7	1-methyl-3-n-propylbenzene	~~5.92~~ 7.10
01074-55-1	1-methyl-4-n-propylbenzene	~~5.92~~ 4.43
00135-01-3	1,2-diethylbenzene	~~5.92~~ 5.49
01074-17-5	1-methyl-2-n-propylbenzene	~~5.92~~ 5.49
01758-88-9	1,4-dimethyl-2-ethylbenzene	~~8.86~~ 7.55
00874-41-9	1,3-dimethyl-4-ethylbenzene	~~8.86~~ 7.55
00934-80-5	1,2-dimethyl-4-ethylbenzene	~~8.86~~ 7.55
02870-04-4	1,3-dimethyl-2-ethylbenzene	~~8.86~~ 10.15
01120-21-4	n-undecane (hendecane)	~~0.74~~ 0.61
00933-98-2	1,2-dimethyl-3-ethylbenzene	~~8.86~~ 10.15
00095-93-2	1,2,4,5-tetramethylbenzene	~~8.86~~ 9.26
01595-11-5	1-methyl-2-n-butylbenzene	~~5.35~~ 4.73
00527-53-7	1,2,3,5-tetramethylbenzene	~~8.86~~ 9.26
01074-92-6	1-(1,1-dimethylethyl)-2-methylbenzene	~~5.35~~ 4.73
00488-23-3	1,2,3,4-tetramethylbenzene	~~8.86~~ 9.26
00538-68-1	n-pentylbenzene	~~1.78~~ 2.12
00098-19-1	1-(1,1-dimethylethyl)-3,5-DMbenzene	~~7.33~~ 8.02
00091-20-3	naphthalene	~~3.26~~ 3.34
00112-40-3	n-dodecane	~~0.66~~ 0.55

CAS #	COMPOUND	MIR

Carbonyl Compounds

CAS #	COMPOUND	MIR
00050-00-0	formaldehyde	~~8.97~~ 9.46
00075-07-0	acetaldehyde	~~6.84~~ 6.54
00107-02-8	acrolein	~~7.60~~ 7.45
00067-64-1	acetone	~~0.43~~ 0.36
00123-38-6	propionaldehyde	~~7.89~~ 7.08
00123-72-8	butyraldehyde	~~6.74~~ 5.97
00066-25-1	hexanaldehyde	~~4.98~~ 4.35
00100-52-7	benzaldehyde	0.00
00078-93-3	methyl ethyl ketone (2-butanone)	~~1.49~~ 1.48
00078-85-3	methacrolein	~~6.23~~ 6.01
04170-30-3	crotonaldehyde	~~10.07~~ 9.39
00110-62-3	valeraldehyde	~~5.76~~ 5.08
00620-23-5	m-tolualdehyde	0.00

List of Compounds
(Listed by CAS number)

00050-00-0	formaldehyde
00064-17-5	ethanol
00066-25-1	hexanaldehyde
00067-56-1	methanol
00067-64-1	acetone
00071-43-2	benzene
00074-84-0	ethane
00074-85-1	ethene
00074-86-2	ethyne
00074-98-6	propane
00074-99-7	1-propyne
00075-07-0	acetaldehyde
00075-28-5	2-methylpropane
00075-83-2	2,2-dimethylbutane
00078-78-4	2-methylbutane
00078-79-5	2-methyl-1,3-butadiene
00078-85-3	methacrolein
00078-93-3	methyl ethyl ketone (2-butanone)
00079-29-8	2,3-dimethylbutane
00091-20-3	naphthalene
00095-47-6	o-xylene
00095-63-6	1,2,4-trimethylbenzene
00095-93-2	1,2,4,5-tetramethylbenzene
00096-14-0	3-methylpentane
00096-37-7	methylcyclopentane
00098-19-1	1-(1,1-dimethylethyl)-3,5-dimethylbenzene
00098-82-8	(1-methylethyl)benzene
00099-87-6	1-methyl-4-(1-methylethyl)benzene
00100-41-4	ethylbenzene
00100-42-5	stryrene (ethenylbenzene)
00100-52-7	benzaldehyde
00103-65-1	n-propylbenzene
00105-05-5	1,4-diethylbenzene
00106-97-8	n-butane
00106-98-9	1-butene
00106-99-0	1,3-butadiene
00107-00-6	1-butyne
00107-02-8	acrolein
00107-39-1	2,4,4-trimethyl-1-pentene
00107-40-4	2,4,4-trimethyl-2-pentene
00107-83-5	2-methylpentane
00108-08-7	2,4-dimethylpentane

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00108-38-3	m- & p-xylene
00108-67-8	1,3,5-trimethylbenzene
00108-87-2	methylcyclohexane
00108-88-3	toluene
00109-66-0	n-pentane
00109-67-1	1-pentene
00110-54-3	n-hexane
00110-62-3	valeraldehyde
00110-82-7	cyclohexane
00110-83-8	cyclohexene
00111-65-9	n-octane
00111-66-0	1-octene
00111-84-2	n-nonane
00112-40-3	n-dodecane
00115-07-1	propene
00115-11-7	2-methylpropene
00123-38-6	propionaldehyde
00123-72-8	butyraldehyde
00124-11-8	1-nonene
00124-18-5	n-decane
00135-01-3	1,2-diethylbenzene
00135-98-8	(1-methylpropyl)benzene
00141-93-5	1,3-diethylbenzene
00142-29-0	cyclopentene
00142-82-5	n-heptane
00287-92-3	cyclopentane
00463-49-0	1,2-propadiene
00463-82-1	2,2-dimethylpropane
00464-06-2	2,2,3-trimethylbutane
00488-23-3	1,2,3,4-tetramethylbenzene
00496-11-7	2,3-dihydroindene (indan)
00503-17-3	2-butyne
00513-35-9	2-methyl-2-butene
00526-73-8	1,2,3-trimethylbenzene
00527-53-7	1,2,3,5-tetramethylbenzene
00527-84-4	1-methyl-2-(1-methylethyl)benzene
00535-77-3	1-methyl-3-(1-methylethyl)benzene
00538-68-1	n-pentylbenzene
00538-93-2	(2-methylpropyl)benzene
00540-84-1	2,2,4-trimethylpentane
00542-92-7	1,3-cyclopentadiene
00558-37-2	3,3-dimethyl-1-butene
00560-21-4	2,3,3-trimethylpentane
00562-49-2	3,3-dimethylpentane
00563-16-6	3,3-dimethylhexane
00563-45-1	3-methyl-1-butene

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00563-46-2	2-methyl-1-butene
00565-59-3	2,3-dimethylpentane
00565-75-3	2,3,4-trimethylpentane
00584-94-1	2,3-dimethylhexane
00589-34-4	3-methylhexane
00589-43-5	2,4-dimethylhexane
00589-53-7	4-methylheptane
00589-81-1	3-methylheptane
00590-18-1	cis-2-butene
00590-35-2	2,2-dimethylpentane
00590-73-8	2,2-dimethylhexane
00591-76-4	2-methylhexane
00592-13-2	2,5-dimethylhexane
00592-27-8	2-methylheptane
00592-41-6	1-hexene
00592-76-7	1-heptene
00611-14-3	1-methyl-2-ethylbenzene
00616-12-6	3-methyl-trans-2-pentene
00617-78-7	3-ethylpentane
00620-14-4	1-methyl-3-ethylbenzene
00620-23-5	m-tolualdehyde
00622-96-8	1-methyl-4-ethylbenzene
00624-64-6	trans-2-butene
00625-27-4	2-methyl-2-pentene
00627-20-3	cis-2-pentene
00637-92-3	1-ethyl-tert-butyl-ether
00638-04-0	cis-1,3-dimethylcyclohexane
00646-04-8	trans-2-pentene
00674-76-0	4-methyl-trans-2-pentene
00689-97-4	1-buten-3-yne
00691-37-2	4-methyl-1-pentene
00691-38-3	4-methyl-cis-2-pentene
00693-89-0	1-methylcyclopentene
00760-20-3	3-methyl-1-pentene
00763-29-1	2-methyl-1-pentene
00816-79-5	3-ethyl-2-pentene
00822-50-4	trans-1,2-dimethylcyclopentane
00874-41-9	1,3-dimethyl-4-ethylbenzene
00922-62-3	3-methyl-cis-2-pentene
00926-82-9	3,5-dimethylheptane
00933-98-2	1,2-dimethyl-3-ethylbenzene
00934-80-5	1,2-dimethyl-4-ethylbenzene
01069-53-0	2,3,5-trimethylhexane
01072-05-5	2,6-dimethylheptane
01074-17-5	1-methyl-2-n-propylbenzene
01074-43-7	1-methyl-3-n-propylbenzene

01074-55-1	1-methyl-4-n-propylbenzene
01074-92-6	1-(1,1-dimethylethyl)-2-methylbenzene
01120-21-4	n-undecane (hendecane)
01120-62-3	3-methylcyclopentene
01595-11-5	1-methyl-2-n-butylbenzene
01634-04-4	1-methyl-tert-butyl-ether
01640-89-7	ethylcyclopentane
01678-91-7	ethylcyclohexane
01758-88-9	1,4-dimethyl-2-ethylbenzene
01759-58-6	trans-1,3-dimethylcyclopentane
02051-30-1	2,6-dimethyloctane
02207-01-4	cis-1,2-dimethylcyclohexane
02207-03-6	trans-1,3-dimethylcyclohexane
02207-04-7	trans-1,4-dimethylcyclohexane
02213-23-2	2,4-dimethylheptane
02216-33-3	3-methyloctane
02216-34-4	4-methyloctane
02532-58-3	cis-1,3-dimethylcyclopentane
02613-65-2	trans-1-methyl-3-ethylcyclopentane
02738-19-4	2-methyl-2-hexene
02815-58-9	1,2,4-trimethylcyclopentane
02870-04-4	1,3-dimethyl-2-ethylbenzene
03074-71-3	2,3-dimethylheptane
03221-61-2	2-methyloctane
03404-61-3	3-methyl-1-hexene
03522-94-9	2,2,5-trimethylhexane
03899-36-3	3-methyl-trans-3-hexene
04032-94-4	2,4-dimethyloctane
04050-45-7	trans-2-hexene
04170-30-3	crotonaldehyde
06443-92-1	cis-2-heptene
07385-78-6	3,4-dimethyl-1-pentene
07642-04-8	cis-2-octene
07642-09-3	cis-3-hexene
07688-21-3	cis-2-hexene
10574-37-5	2,3-dimethyl-2-pentene
13269-52-8	trans-3-hexene
13389-42-9	trans-2-octene
14686-13-6	trans-2-heptene
14686-14-7	trans-3-heptene
14850-23-8	trans-4-octene
15869-87-1	2,2-dimethyloctane
15890-40-1	(1a,2a,3b)-1,2,3-trimethylcyclopentane
16747-50-5	cis-1-methyl-3-ethylcyclopentane

APPENDIX 2

DEFINITIONS AND COMMONLY USED ABBREVIATIONS

I.   The abbreviations and definitions set forth in this section apply to Parts A through G of these test procedures:

ASTM   =   American Society for Testing and Materials

Carbon No.   =   number of carbon atoms in the hydrocarbon or organic compound being measured.

CCR   =   California Code of Regulations

CH_3OH_d =   the methanol concentration in the dilution air as determined from the dilution air methanol sample using the procedure specified in Method No. 1001, ppmC.

CH_3OH_e =   the methanol concentration in the dilute exhaust as determined from the dilute exhaust methanol sample using the procedure specified in Method No. 1001, ppmC.

CH_{4d} =   the methane concentration in the dilution air, ppmC.

CH_{4e} =   the methane concentration in the dilute exhaust, ppmC.

$C_2H_5OH_d$ =   the ethanol concentration in the dilution air as determined from the dilution air ethanol sample using the procedure specified in Method No. 1001, ppmC.

$C_2H_5OH_e$ =   the ethanol concentration in the dilute exhaust as determined from the dilute exhaust ethanol sample using the procedure specified in Method No. 1001, ppmC.

CNG   =   compressed natural gas

CO_e =   the carbon monoxide concentration in the dilute exhaust corrected for carbon dioxide and water removal, ppm.

CO_{em} =   the carbon monoxide concentration in the dilute exhaust uncorrected for carbon dioxide and water removal, ppm.

CO_{2e} =   the carbon dioxide concentration in the dilute exhaust, %.

CVS   =   constant volume sampler

$D_{\text{phase n}}$	=	the distance driven by the test vehicle on a chassis dynamometer during test phase n (where n is either 1, 2, or 3), mile.
~~Dens_{ROH}~~	~~=~~	~~density of alcohol, g/mL.~~
DF	=	dilution factor (see Dilution Factor Calculation).
FID	=	flame ionization detector
FID THC_d	=	the total hydrocarbon concentration including methane and methanol (for methanol-fueled engines) or ethanol (for ethanol-fueled engines) in the dilution air as measured by the FID, ppmC.
FID THC_e	=	the total hydrocarbon concentration including methane and methanol (for methanol-dueled engines) or ethanol (for ethanol-fueled engines) in the dilution exhaust as measured by the FID, ppmC.
FTP	=	Federal Test Procedure
GC	=	gas chromatograph
GC/MS	=	gas chromatography/mass spectrometry
HC_{conc}	=	net concentration of an HC compound in the dilute exhaust corrected for background per test phase, ppbC.
HC_d	=	composite concentration of an HC compound in the dilution air (background) for all three test phases as determined from the composite dilution air sample using the procedure specified in Method No. 1002 and Method No. 1003, ppbC.
HC_{dens}	=	mass per unit volume of an HC compound corrected to standard conditions (293.16 K and 760 mm Hg) g/ft^3.
HC_e	=	concentration of an HC compound in the dilute exhaust per test phase as determined from the dilute exhaust sample using the procedure specific in Method No. 1002 and Method No. 1003, ppbC.
$\text{HC}_{\text{mass n}}$	=	mass emissions of an HC compound per test phase n (where n is either 1, 2, or 3), mg.

HC$_{wm}$	=	total weighted mass of an HC compound per mile, g/mile.
HCHO$_e$	=	formaldehyde concentration in the dilute exhaust as determined from the dilute exhaust carbonyl sample using the procedure specified in Method No 1004, ppm.
HCR	=	the hydrogen-to-carbon ratio for the fuel used.
HPLC	=	high performance liquid chromatography
Iconc$_{blk}$	=	concentration of the blank cartridge, µg/mL
Iconc$_{cd}$	=	total concentration of carbonyl compound extracted from both cartridges for the dilution air, µg/mL
Iconc$_{ce}$	=	total concentration of carbonyl compound extracted from both cartridges for the diluted exhaust, µg/mL
Iconc$_{d1}$	=	dilution air (background) alcohol concentration in the primary impinger for all three test phases as determined by the procedure specified in Method No. 1001, µg/mL.
Iconc$_{d2}$	=	dilution air (background) alcohol concentration in the secondary impinger for all three test phases as determined by the procedure specified in Method No. 1001, µg/mL.
Iconc$_{e1}$	=	dilute exhaust alcohol concentration in the primary impinger per test phase as determined by the procedure specified in Method No. 1001, µg/mL.
Iconc$_{e2}$	=	dilute exhaust alcohol concentration in the secondary impinger per test phase as determined by the procedure specified in Method No. 1001, µg/mL.
Imass$_d$	=	total mass of an alcohol or carbonyl compound collected from the dilution air (background) in both primary and secondary impingers/cartridges for all three test phases as determined by the procedure specified in Method No. 1001 (alcohol) or Method No. 1004 (carbonyl), µg.
Imass$_e$	=	total mass of an alcohol or carbonyl compound collected from the dilute exhaust in both primary and secondary impingers/cartridges per test phase as determined by the procedure specified in Method No. 1001 (alcohol) or Method No. 1004 (carbonyl), µg.

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Itemp$_d$	=	dilution air temperature at the flowmeter inlet for impinger/cartridge sampling, ^{o}K.
Itemp$_e$	=	dilute exhaust temperature at the flowmeter inlet for impinger/cartridge sampling, ^{o}K.
Ivol$_c$	=	elution volume of the cartridge, mL (<u>For example,</u> ~~T~~the cartridge is extracted with 5 mL acetonitrile, but 0.6 mL is retained in the cartridge, so the elution volume is 4.4 mL.)
Ivol$_d$	=	total volume of dilution air (background) drawn through the impingers/cartridges for all three test phases corrected to standard conditions (293.16^{o}K and 760 mm Hg), liter.
Ivol$_{dm}$	=	total volume of dilution air (background) drawn through the impingers/cartridges for all three test phases as measured during testing, liter.
Ivol$_e$	=	total volume of dilute exhaust drawn through the impingers/cartridges per test phase corrected to standard conditions (293.16^{o}K and 760 mm Hg), liter.
Ivol$_{em}$	=	total volume of dilute exhaust drawn through the impingers/cartridges per test phase as measured during testing, liter.
Ivol$_r$	=	volume of the reagent used in an impinger, mL.
LOD	=	limit of detection
LPG	=	liquified petroleum gas
Mol. Vol.	=	molecular volume which is 24.055 liter/mole at standard conditions (293.16^{o}K and 760 mm Hg).
Mol. Wt.	=	molecular weight of the compound being measured, g/mole.
NIST	=	National Institute of Standards and Technology
NMHC	=	non-methane hydrocarbons
NMHC$_{conc}$	=	the non-methane hydrocarbon concentration in the dilute exhaust corrected for background, ppmC.

NMHC$_d$	=	the non-methane hydrocarbon concentration in the dilution air corrected for methane and alcohol removal, ppmC.
NMHC$_{dens}$	=	the mass per unit volume of non-methane hydrocarbon corrected to standard conditions (16.33 g/ft^3 at 293.16^{o}K and 760 mm Hg assuming a C:H ratio of 1:1.85 for gasoline; 16.78 g/ft^3 at 293.16^{o}K and 760 mm HG assuming a C:H ratio of 1:1.94 for Phase 2 reformulated gasoline; 19.52 g/ft^3 at 293.16^{o}K and 760 mm HG assuming a C:H ratio of 1:3.78 for natural gas; and 17.26 g/ft^3 for LPG at 293.16^{o}K and 760 mm Hg assuming a C:H ratio of 1:2.64), g/ft^3-.
NMHC$_e$	=	non-methane hydrocarbon concentration in the dilute exhaust corrected for methane and alcohol removal, ppmC.
NMHC$_{mass\ n}$	=	the mass emission of non-methane hydrocarbon per test phase n (where n is either 1, 2, or 3), g.
NMHC$_{wm}$	=	the total weighted mass of non-methane hydrocarbon per mile for all three phases of the FTP, g/mile.
NONMHC$_{mass\ n}$	=	the mass emission of non-oxygenated non-methane hydrocarbon per test phase n (where n is either 1, 2, or 3), g.
NONMHC$_{wm}$	=	the total weighted mass of non-oxygenated non-methane hydrocarbon per mile for all three phases of the FTP, g/mile.
NMOG	=	non-methane organic gases
P$_B$	=	barometric pressure during testing, mm Hg.
PID	=	photoionization detector
PLOT	=	porous layer open tubular
R$_a$	=	the relative humidity of the ambient air, %.
r$_{CH_3OH}$	=	the FID response factor to methanol (see CFR 40, 86.121-90(c)).
r$_{CH_4}$	=	the FID response factor to methane (see Part B, "Determination of NMHC by FID").
r$_{C_2H_5OH}$	=	the FID response factor to ethanol (same procedure for methanol response factor, see CFR 40, 86.121-90(c)).

r_{ROH}	=	the FID response factor to an alcohol
r_{RHO}	=	the FID response factor to carbonyl compound
RHO	=	generic symbol representing a carbonyl compound such as formaldehyde, acetaldehyde, acetone, etc.
RHO_{conc}	=	net concentration of a carbonyl compound in the dilute exhaust corrected for background per test phase, ppm.
RHO_d	=	composite concentration of a carbonyl compound in the dilution air (background) for all three test phases, ppm.
RHO_{dens}	=	mass per unit volume of a carbonyl compound corrected to standard conditions (293.16^{o}K and 760 mm Hg), g/ft^3.
RHO_e	=	concentration of a carbonyl compound in the dilute exhaust per test phase, ppm.
$RHO_{mass\ n}$	=	mass emissions of a carbonyl compound per test phase n (where n is either 1, 2, or 3), g.
RHO_{wm}	=	total weighted mass emissions of a carbonyl compound per mile, g/mile.
ROH	=	generic symbol representing an alcohol compound such as methanol or ethanol.
ROH_{conc}	=	net concentration of an alcohol compound in the dilute exhaust corrected for background per test phase, ppm.
ROH_d	=	composite concentration of an alcohol compound in the dilution air (background) for all three test phases, ppm.
ROH_{dens}	=	mass per unit volume of an alcohol compound corrected to standard conditions (293.16^{o}K and 760 mm Hg), g/ft^3.
ROH_e	=	concentration of an alcohol compound in the dilute exhaust per test phase, ppmC.
$ROH_{mass\ n}$	=	mass emissions of an alcohol compound per test phase n (where n is either 1, 2, or 3), g.
ROH_{wm}	=	total weighted mass emissions of an alcohol compound per mile, g/mile.

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SAE   =   Society of Automotive Engineers

SRM   =   Standard Reference Material

VMIX   =   the total dilute exhaust volume measured per test phase and corrected to standard conditions (293.16°K and 760 mm Hg), ft^3.

II.   The following list is commonly used measurement abbreviations:

g   =   gram
µg   =   microgram
m   =   meter
cm   =   centimeter
µm   =   micrometer
µ   =   micron
L   =   liter
mL   =   milliliter
µL   =   microliter
ppb   =   parts per billion.
ppbC   =   parts per billion carbon equivalent.
ppm   =   parts per million.
ppmC   =   parts per million carbon equivalent.

APPENDIX 3

REFERENCES

[1]   Code of Federal Regulations, Title 40, Part 86, Subpart B

[2]   SAE J254, "Instrumentation and Techniques for Exhaust Gas Emissions Measurement"

[3]   SAE J1094a, "Constant Volume Sampler System for Exhaust Emissions Measurement"

[4]   SAE 770141, "Optimization of a Flame Ionization Detector for Determination of Hydrocarbons in Diluted Automotive Exhausts". G.D. Reschke, Vehicle Emissions Laboratory, General Motors Proving Ground

[5]   SAE J1154, "Methane Measurement Using Gas Chromatography," (revised December 1991)

[6]   U.S. Environmental Protection Agency, <u>Characterization of Exhaust Emissions from Methanol and Gasoline Fueled Automobiles</u>, EPA 460/3-82-004.

[7]   U.S. Environmental Protection Agency, <u>Compendium of Methods for the Determination of Toxic Organic Compounds in Ambient Air</u>, (Method T03-15) EPA-600/4-89-017 Research Triangle Park, North Carolina, June, 1989.

[8]   Standard Test Method for C_1 through C_6 Hydrocarbons in the Atmosphere by Gas Chromatography, American Standards for Testing Materials (ASTM) Standards on Chromatography (1981).

[9]   U.S. Environmental Protection Agency, <u>Compendium of Methods for the Determination of Toxic Organic Compounds in Ambient Air</u>, (Method T03-15) EPA-600/4-84-041 Research Triangle Park, North Carolina, April, 1989.

[10]   Hull, L.A., <u>Procedures for 2,4-Dinitrophenylhydrazone Aldehyde-Ketone Air Analysis</u>, Internal Report at U.S. EPA.

[11]   Shriner, R.L. and Fuson, R.C., <u>Identification of Organic Compounds</u>, 2nd. Ed., John Wiley and Sons, Inc., 1940, p. 143.

[12]   Keith, L. H., Taylor, J.K., et al, "Principles of Environmental Analysis", <u>Analytical Chemistry</u>, Vol. 55, No. 14, December 1983.

Appendix 3